Part III

Restoration Design

8

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Design can be defined as the intentional shaping of matter, energy, and process to meet an expressed need. Planning and design connect natural processes and cultural needs through exchanges of materials, flows of energy, and choices of land use and management. One test of a successful stream corridor design is how well the restored system sustains itself over time while accommodating identified needs.

To achieve success, those carrying out restoration design and implementation in variable-land-use settings must understand the stream corridor, watershed, and landscape as a

*complex of working ecosystems that influence and are influenced by neighboring ecosystems (**Figure 8.1**). The probability of achieving long-term, self-sustaining functions across this spatial complex increases with an understanding of these relationships, a common language for expressing them, and subsequent response. Designing to achieve stream- or corridor-specific solutions might not resolve problems or recognize opportunities in the landscape.*

Stream corridor restoration design is still largely in an experimental stage. It is known however, that restoration design must consider site-specific or local conditions to be successful. That is, the design criteria, standards, and specifications should be for the specific project in a specific physical, climatic, and geographic location. These initiatives, however, can and should work with, rather than against, the larger systems of which they are an integral part.

This approach produces multiple benefits, including:

- *A healthy, sustainable pattern of land uses across the landscape.*

- *Improved natural resource quality and quantity.*

Figure 8.1: Stream running through a wet meadow.
Restoration design must consider site-specific conditions as an integral part of larger systems.

- *Restored and protected stream corridors and associated ecosystems.*
- *A diversity of native plants and animals.*
- *A gene pool that promotes hardiness, disease resistance, and adaptability.*
- *A sense of stewardship for private landowners and the public.*
- *Improved management measures that avoid narrowly focused and fragmented land treatment.*

Building on information presented in Parts I and II, this chapter contains design guidance and techniques to address changes caused by major disturbances and to restore stream corridor structure and function to a desired level. It begins with larger-scale influences that design may have on stream corridor ecosystems, offers design guidance primarily at the stream corridor and stream scales, and concludes with land use scenarios.

The chapter is divided into seven sections.

Section 8.A: Valley Form, Connectivity, and Dimension

This section focuses on restoring structural characteristics that prevail at the stream corridor and landscape scales.

Section 8.B: Soil Properties

The restoration of soil properties that are critical to stream corridor structure and functions are addressed in this section.

Section 8.C: Vegetative Communities

Restoring vegetative communities is a highly visible and integral component of a functioning stream corridor.

Section 8.D: Habitat Measures

This section presents design guidance for some habitat measures. They are often integral parts of stream corridor structure and functions.

Section 8.E: Stream Channel Restoration

Restoring stream channel structure and functions is often a fundamental step in restoring stream corridors.

Section 8.F: Streambank Restoration

This section focuses on design guidelines and related techniques for streambank stabilization. These measures can help reduce surface runoff and sediment transport to the stream.

Section 8.G: Instream Habitat Recovery

Restoring instream habitat structure and functions is often a key component of stream corridor restoration.

Section 8.H: Land Use Scenarios

This final section offers broad design concepts in the context of major land use scenarios.

"Leave It Alone / Let It Heal Itself"

There is a renewed emphasis on recovering damaged rivers (Barinaga 1996). Along with this concern, however, people should be reminded periodically that they serve as stewards of watersheds, not just tinkerers with stream sites. Streams in pristine condition, for example, should not be artificially "improved" by active rehabilitation methods.

At the other end of the spectrum, and particularly where degradation is caused by off-stream activities, the best solution to a river management problem might be to remove the problem source and "let it heal itself." Unfortunately, in severely degraded streams this process can take a long, time. Therefore the "leave it alone" concept can be the most difficult approach for people to accept (Gordon et al. 1992).

8.A Valley Form, Connectivity, and Dimension

Valley form, connectivity, and dimension are variable structural characteristics that determine the interrelationship of functions at multiple scales. Valley intersections (nodes) with tributary stream corridors, slope of valley sides, and floodplain gradient are characteristics of valley form that influence many functions (**Figure 8.2**).

The broad concept of connectivity, as opposed to fragmentation, involves linkages of habitats, species, communities, and ecological processes across multiple scales (Noss 1991). Dimension encompasses width, linearity, and edge effect, which are critical for movement of species, materials, and energy within the stream corridor and to or from ecosystems in the surrounding landscape. Design should therefore address these large-scale characteristics and their effect on functions.

Valley Form

In some cases, entire stream valleys have changed to the point of obscuring geomorphic boundaries, making stream corridor restoration difficult. Volcanoes, earthquakes, and landslides are examples of natural disturbances that cause changes in valley form. Encroachment and filling of floodplains are among the human-induced disturbances that modify valley shape.

Stream Corridor Connectivity and Dimension

Connectivity and dimensions of the stream corridor present a set of design-related decisions to be made. How wide should the corridor be? How

Figure 8.2: Stream corridors.
(a) Stream valley side slopes and (b) floodplain gradients influence stream corridor function.

(a)

(b)

long should the corridor be? What if there are gaps in the corridor? These structural characteristics have a significant impact on corridor functions. The width, length, and connectivity of existing or potential stream corridor vegetation, for example, are critical to

habitat functions within the corridor and adjacent ecosystems.

Generally, the widest and most contiguous stream corridor which achieves habitat, conduit, filter, and other functions (see Chapter 2) should be an ecologically derived goal of restoration. Thresholds for each function are likely found at different corridor widths. The appropriate width varies according to soil type, with steep slopes requiring a wider corridor for filter functions. A conservative indicator of effective corridor width is whether a stream corridor can significantly prevent chemical contaminants contained in runoff from reaching the stream (Forman 1995).

As discussed in Chapter 1, the corridor should extend across the stream, its banks, the floodplain, and the valley slopes. It should also include a portion of upland for the entire stream length to maintain functional integrity (Forman and Godron 1986).

A contiguous, wide stream corridor might not be achievable, however, particularly where competing land uses prevail. In these cases, a ladder pattern of natural habitat crossing the floodplain and connecting the upland segments might facilitate sediment trapping during floods and provide hydraulic storage and organic matter for the stream system (Dramstad et al. 1996).

Figure 8.3 presents an example of these connections. The open areas within the ladder pattern are representative of areas that are unavailable for restoration because of competing land uses.

Innovative management practices that serve the functions of the corridor beyond land ownership boundaries can often be prescribed where land owners are supportive of restoration. Altering land cover, reducing chemical inputs, carefully timed mowing, and other management practices can reduce disturbance in the corridor.

Practical considerations may restrict restoration to a zone of predefined width adjacent to the stream. Although often unavoidable, such restrictions tend to result in underrepresentation of older, off-channel environments that support vegetation different from that in stream-front communities. Restricting restoration to a narrow part of the stream corridor usually does not restore the full horizontal diversity of broad floodplains, nor does it fully accommodate functions that occur during flood events, such as use of the floodplain by aquatic species (Wharton et al. 1982).

In floodplains where extensive subsurface hydrologic connections exist, limiting restoration to streamside buffer zones is not recommended since significant amounts of energy, nutrient transformation, and invertebrate activities can occur at great distances
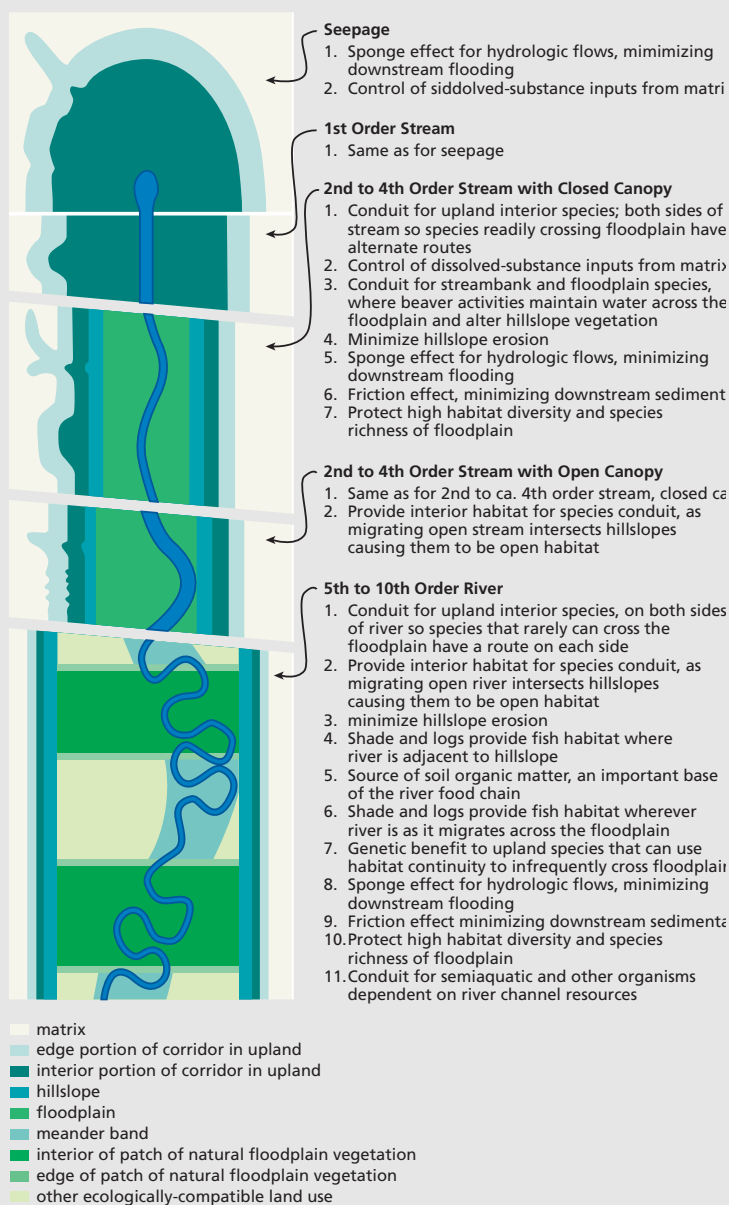
**Figure 8.3:
Connections across a
stream corridor.**

*A ladder pattern of natural
habitat can restore
structure and functions
where competing land
uses prevail.*

**Adapted from *Ecology of
Greenways: Design and
Function of Linear
Conservation Areas*.
Edited by Smith and
Hellmund. ©University of
Minnesota Press 1993.**
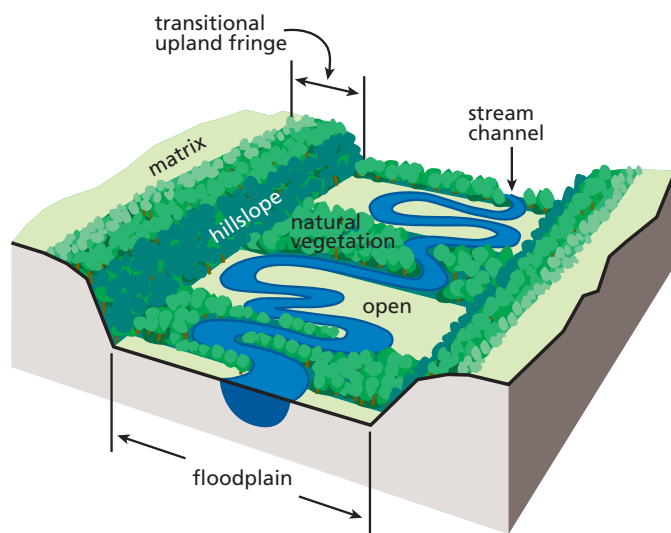
Corridor Width Variables

The minimum width of stream corridors based on ecological criteria (**Figure 8.4**). Five basic situations in a river system are identified, progressing from seepage to river. The key variables determining minimum corridor width are listed under each.

Figure 8.4: Factors for determining minimum corridor widths.
Stream corridor functions are directly influenced by corridor width.
From Forman 1995. Reprinted with permission of Cambridge University Press.

Seepage
1. Sponge effect for hydrologic flows, mimimizing downstream flooding
2. Control of siddolved-substance inputs from matri\

1st Order Stream
1. Same as for seepage

2nd to 4th Order Stream with Closed Canopy
1. Conduit for upland interior species; both sides of stream so species readily crossing floodplain have alternate routes
2. Control of dissolved-substance inputs from matri\
3. Conduit for streambank and floodplain species, where beaver activities maintain water across the floodplain and alter hillslope vegetation
4. Minimize hillslope erosion
5. Sponge effect for hydrologic flows, minimizing downstream flooding
6. Friction effect, minimizing downstream sediment
7. Protect high habitat diversity and species richness of floodplain

2nd to 4th Order Stream with Open Canopy
1. Same as for 2nd to ca. 4th order stream, closed ca
2. Provide interior habitat for species conduit, as migrating open stream intersects hillslopes causing them to be open habitat

5th to 10th Order River
1. Conduit for upland interior species, on both sides of river so species that rarely can cross the floodplain have a route on each side
2. Provide interior habitat for species conduit, as migrating open river intersects hillslopes causing them to be open habitat
3. minimize hillslope erosion
4. Shade and logs provide fish habitat where river is adjacent to hillslope
5. Source of soil organic matter, an important base of the river food chain
6. Shade and logs provide fish habitat wherever river is as it migrates across the floodplain
7. Genetic benefit to upland species that can use habitat continuity to infrequently cross floodplai\
8. Sponge effect for hydrologic flows, minimizing downstream flooding
9. Friction effect minimizing downstream sedimenta\
10. Protect high habitat diversity and species richness of floodplain
11. Conduit for semiaquatic and other organisms dependent on river channel resources

- matrix
- edge portion of corridor in upland
- interior portion of corridor in upland
- hillslope
- floodplain
- meander band
- interior of patch of natural floodplain vegetation
- edge of patch of natural floodplain vegetation
- other ecologically-compatible land use

from the stream channel outside the buffer areas (Sedell et al. 1990). Similarly, failure to anticipate channel migration or periodic beaver activity might result in a corridor that does not accommodate fundamental dynamic processes (Malanson 1993).

As previously discussed, restoration of an ecologically effective stream corridor requires consideration of uplands adjacent to the channel and floodplain. Hillslopes might be a source area for water maintaining floodplain wetlands, a sediment source for channels on bedrock, and the principal source of organic debris in high-gradient streams.

Despite these considerations, stream corridors are often wrongly viewed as consisting of only the channel and an adjacent vegetative buffer. The width of the buffer is determined by specific objectives such as control of agricultural runoff or habitat requirements of particular animal species. This narrow definition obviously does not fully accommodate the extent of the functions of a stream corridor; but where the corridor is limited by immovable resource uses, it often becomes a part of a restoration strategy.

Cognitive Approach: The Reference Stream Corridor

Ideal stream corridor widths, as previously defined, are not always achievable in the restoration design. A local *reference stream corridor* might provide dimensions for designing the restoration.

Examination of landscape patterns is beneficial in identifying a reference stream corridor. The reference should provide information about gap width, landform, species requirements,

vegetative structure, and boundary characteristics of the stream corridor (**Figure 8.5**).

Restoration objectives determine the desired levels of functions specified by the restoration design. If a nearby stream corridor in a similar landscape setting and with similar land use variables provides these functions adequately, it can be used to indicate the connectivity and width attributes that should be part of the design.

Analytical Approach: Functional Requirements of a Target Species

The restoration plan objectives can be used to determine dimensions for the stream corridor restoration. If, for example, a particular species requires that the corridor offer interior habitat, the corridor width is sized to provide the necessary habitat. The requirements of the most sensitive species typically are used for optimum corridor dimensions. When these dimensions extend beyond the land base available for restoration, management of adjacent land uses becomes a tool for making the corridor effectively wider than the project parameters.

Figure 8.5: A maple in a New Mexico floodplain.
A rare occurrence of a remnant population may reflect desired conditions in a reference stream corridor.

Optimum corridor dimensions can be achieved through collaboration with individuals and organizations who have management authority over adjacent lands. Dimensions include width of edge effect associated with boundaries of the corridor and pattern variations within the corridor, maximum acceptable width of gaps within the corridor, and maximum number of gaps per unit length of corridor.

Designing for Drainage and Topography

The stream corridor is dependent on interactions with the stream to sustain its character and functions (see Chapter 2). Therefore, to the extent feasible, the restoration process should include blockage of artificial drainage systems, removal or setback of artificial levees, and restoration of natural patterns of floodplain topography, unless these actions conflict with other social or environmental objectives (e.g., flooding or habitat).

Restoration of microrelief is particularly important where natural flooding has been reduced or curtailed because a topographically complex floodplain supports a mosaic of plant communities and ecosystem functions as a result of differential ponding of rainfall and interception of ground water. Microrelief restoration can be accomplished by selective excavation of historic features within the floodplain such as natural wetlands, levees, oxbows, and abandoned channels. Aerial photography and remotely sensed data, as well as observations in reference corridors, provide an indication of the distribution and dimensions of typical floodplain microrelief features.

8.B Soil Properties

Stream corridor functions depend not only on the connectivity and dimensions of the stream corridor, but also on its soils and associated vegetation. The variable nature of soils across and along stream corridors results in diverse plant communities (**Figure 8.6**). When designing stream corridor restoration measures, it is important to carefully analyze the soils and their related potentials and limitations to support diverse native plant and animal communities, as well as for restoration involving channel reconstruction.

Where native floodplain soils remain in place, county soil surveys should be used to determine basic site conditions and fertility and to verify that the proposed plant species to be restored are appropriate. Most sites with fine-textured alluvium will not require supplemental fertilization, or fertilizers might be required only for initial establishment. In these cases excessive fertilization could encourage competing weed species or exotics. Soil should always be tested before making any fertilizer design recommendations.

County soil surveys can provide basic information such as engineering limitations or suitabilities. Site-specific soil samples should, however, be collected and tested when the restoration involves alternatives that include stream reconstruction.

The connections and feedback loops between runoff and the structure and functions of streams are described in Chapter 2. The functions of soil and the connection between soil quality,

Figure 8.6: Distinct vegetation zones along a mountain stream.
Variable soils result in diverse plant communities.

runoff, and water quality are also established in that chapter. These connections need to be identified and considered in any stream corridor restoration plan and design. For all land uses, emphasis needs to be placed on implementing conservation land treatment that promotes soil quality and the ability of the soils to carry out four major functions:

- Regulating and partitioning the flow of water (a conduit and filter function).

- Storing and cycling nutrients and other chemicals (a sink and filter function).

- Filtering, buffering, degrading, immobilizing, and detoxifying organic and inorganic materials (a filter, sink, and barrier function).

Figure 8.7: Compaction of streamside soil.
Compact soils may require deep plowing, ripping, or vegetative practices to break up the impermeable layer.

- Supporting biological activity in the landscape (a source and habitat function).

References such as *Field Office Technical Guide* (USDA-NRCS) contain guidance on the planning and selection of conservation practices and are available at most county offices.

Compaction

Soils that have been in row crops or have undergone heavy equipment traffic (such as that associated with construction) can develop a relatively impermeable compacted layer (plow pan or hard pan) that restricts water movement and root penetration (**Figure 8.7**). Such soils might require deep plowing, ripping, or vegetative practices to break up the pan, although even these are sometimes ineffective. Deep plowing is usually expensive and, at least in the East, should be used only if the planting of a species that is able to penetrate the pan layer is not a viable option.

Soil Microfauna

On new or disturbed substrates, or on row-cropped sites, essential soil microorganisms (particularly mycorrhizal fungi) might not exist. These are most effectively replaced by using rooted plant material that is inoculated or naturally infected with appropriate fungi. Stockpiling and reincorporating local topsoils into the substrate prior to planting is also effective (Allen 1995). Particular care should be taken to avoid disturbing large trees or stumps since the soils around and under them are likely source areas for reestablishment of a wide variety of microorganisms. Inoculation can be useful in restoring some soil mycorrhizal fungi for particular species when naturally infected plant stock is unavailable.

Soil Salinity

Soil salinity is another important consideration in restoration because salt accumulation in the soil can restrict plant growth and the establishment of riparian species. High soil salinity is not common in healthy riparian ecosystems where annual spring floods remove excess salts. Soil salinity can also be altered by leaching salts through the soil profile with irrigation (Anderson et al. 1984). Because of agricultural drainage and altered flows due to dam construction, salt accumulation often contributes to riparian plant community declines.

Soil sampling throughout a restoration site may be necessary since salinity can vary across a floodplain, even on sites of less than 20 acres. If salinity is a problem, one must select plant materials adapted to a saline soil environment.

8.C Plant Communities

Vegetation is a fundamental controlling factor in stream corridor function. Habitat, conduit, filter/barrier, source, and sink functions are all critically tied to the vegetative biomass amount, quality, and condition (**Figure 8.8**). Restoration designs should protect existing native vegetation and restore vegetative structure to result in a contiguous and connected stream corridor.

Restoration goals can be general (e.g., returning an area to a reference condition) or specific (e.g., restoring habitats for particular species of interest such as the least Bell's vireo, Vireo *bellii* [Baird and Rieger 1988], or yellow-billed cuckoo, *Coccyzus americana* [Anderson and Laymon 1988]).

Numerous shrubs and trees have been evaluated as restoration candidates, including willows (Svejcar et al. 1992, Hoag 1992, Conroy and Svejcar 1991, Anderson et al. 1978); alder, service-berry, oceanspray, and vine maple (Flessner et al. 1992); cottonwood and poplar (Hoag 1992); Sitka and thinleaf alder (Java and Everett 1992); palo verde and honey mesquite (Anderson et al. 1978); and many others. Selection of vegetative species may be based on the desire to provide habitat for a particular species of interest. The current trend in restoration, however, is to apply a multispecies or ecosystem approach.

Riparian Buffer Strips

Managers of riparian systems have long recognized the importance of *buffer strips*, for the following reasons (USACE 1991):

- Provide shade that reduces water temperature.
- Cause deposition of (i.e., filter) sediments and other contaminants.
- Reduce nutrient loads of streams.
- Stabilize streambanks with vegetation.
- Reduce erosion caused by uncontrolled runoff.
- Provide riparian wildlife habitat.
- Protect fish habitat.
- Maintain aquatic food webs.
- Provide a visually appealing greenbelt.
- Provide recreational opportunities.

Figure 8.8: Stream corridor vegetation. *Vegetation is a fundamental controlling factor in the functioning of stream corridors.*

Although the value of buffer strips is well recognized, criteria for their sizing are variable. In urban stream corridors a wide forest buffer is an essential component of any protection strategy. Its primary value is to provide physical protection for the stream channel from future disturbance or encroachment. A network of buffers acts as the right-of-way for a stream and functions as an integral part of the stream ecosystem.

Often economic and legal considerations have taken precedence over ecological factors. For Vermont, USACE (1991) suggests that narrow strips (100 ft wide) may be adequate to provide many of the functions listed above. For breeding bird populations on Iowa streams, Stauffer and Best (1980) found that minimum strip widths varied from 40 ft for cardinals to 700 ft for scarlet tanagers, American redstarts, and rufous-sided towhees. In urban settings buffer sizing criteria may be based on existing site controls as well as economic, legal, and ecological factors. Practical performance criteria for sizing and managing urban buffers are presented in the box *Designing Urban Stream Buffers*. Clearly, no single recommendation would be suitable for all cases.

Because floodplain/riparian habitats are often small in area when compared to surrounding uplands, meeting the minimum area needs of a species, guild, or community is especially important. Minimum area is the amount of habitat required to support the expected or appropriate use and can vary greatly across species and seasons. For example, Skagen (USGS, Biological Resources Divi-

sion, Ft. Collins, Colorado; unpubl. data) found that, contrary to what might be considered conventional wisdom, extensive stream corridors in southeastern Arizona were not more important to migrating birds than isolated patches or oases of habitat. In fact, oases that were <2.5 miles long and <30 ft in width had more species and higher numbers of nonbreeding migrants than did corridors. Skagen found that the use of oases, as well as corridors, is consistent with the observed patterns of long distance migrants, where migration occurs along broad fronts rather than north-south corridors. Because small and/or isolated patches of habitat can be so important to migrants, riparian restoration efforts should not overlook the important opportunities they afford.

Existing Vegetation

Existing native vegetation should be retained to the extent feasible, as should woody debris and stumps (**Figure 8.9**). In addition to providing habitat and erosion and sediment control, these features provide seed sources and harbor a variety of micro-organisms, as described above. Old fencerows, vegetated stumps and rock piles in fields, and isolated shade trees in pastures should be retained through restoration design, as long as the dominant plant species are native or are unlikely to be competitors in a matrix of native vegetation (e.g., fruit trees).

Nonnative vegetation can prevent establishment of desirable native species or become an unwanted permanent component of stream corridor vegetation. For example,

Designing Urban Stream Buffers

The ability of an *urban stream buffer* to realize its many benefits depends to a large degree on how well it is planned, designed, and maintained. Ten practical performance criteria are offered to govern how a buffer is to be sized, managed, and crossed. The key criteria include:

Criteria 1: minimum total buffer width.

Most local buffer criteria require that development be set back a fixed and uniform distance from the stream channel. Nationally, urban stream buffers range from 20 to 200 ft in width from each side of the stream according to a survey of 36 local buffer programs, with a median of 100 ft (Schueler 1995). In general, a minimum base width of at least 100 feet is recommended to provide adequate stream protection.

Criteria 2: three-zone buffer system:

Effective urban stream buffers have three lateral zones— stream side, middle core, and outer zone. Each zone performs a different function, and has a different width, vegetative target and management scheme. The **stream side zone** protects the physical and ecological integrity of the stream ecosystem. The vegetative target is mature riparian forest that can provide shade, leaf litter, woody debris and erosion protection to the stream. The **middle zone** extends from the outward boundary of the stream side zone, and varies in width, depending on stream order, the extent of the 100-yr floodplain, adjacent steep slopes, and protected wetland areas. Its key functions are to provide further distance between upland development and the stream. The vegetative target for this zone is also mature forest, but some clearing may be allowed for storm water management, access, and recreational uses.

The **outer zone** is the buffer's "buffer," an additional 25-ft setback from the outward edge of the middle zone to the nearest permanent structure. In most instances, it is a residential backyard. The vegetative target for the outer zone is usually turf or lawn, although the property owner is encouraged to plant trees and shrubs, and thus increase the total width of the buffer. Very few uses are restricted in this zone. Indeed, gardening, compost piles, yard wastes, and other common residential activities often will occur in the outer zone.

Criteria 3: predevelopment vegetative target.

The ultimate vegetative target for urban stream buffers should be specified as the predevelopment riparian plant community—usually mature forest. Notable exceptions include prairie streams of the midwest, or arroyos of the arid West, that may have a grass or shrub cover in the riparian zone. In general, the vegetative target should be based on the natural vegetative community present in the floodplain, as determined from reference riparian zones. Turfgrass is allowed for the outer zone of the buffer.

Criteria 4. buffer expansion and contraction.

Many communities require that the minimum width of the buffer be expanded under certain conditions. Specifically, the average width of the middle zone can be expanded to include:

• the full extent of the 100-yr floodplain;

• all undevelopable steep slopes (greater than 25%);

• steep slopes (5 to 25% slope, at four additional ft of slope per one percent increment of slope above 5%); or

• any adjacent delineated wetlands or critical habitats.

Criteria 5: Buffer delineation. Three key decisions must be made when delineating the boundaries of a buffer. At what mapping scale will streams be defined? Where does the stream begin and the buffer end? And from what point should the inner edge of the buffer be measured? Clear and workable delineation criteria should be developed.

Criteria 6. Buffer crossings. Major objectives for stream buffers are to maintain an unbroken corridor of riparian forest and to allow for upstream and downstream fish passage in the stream network. From a practical standpoint, however, it is not always possible to try to meet these goals everywhere along the stream buffer network. Some provision must be made for linear forms of development that must cross the

stream or the buffer, such as roads, bridges, fairways, underground utilities, enclosed storm drains or outfall channels.

Criteria 7. Storm water runoff. Buffers can be an important component of the storm water treatment system at a development site. They cannot, however, treat all the storm water runoff generated within a watershed (generally, a buffer system can only treat runoff from less than 10% of the contributing watershed to the stream). Therefore, some kind of structural BMP must be installed to treat the quantity and quality of storm water runoff from the remaining 90% of the watershed.

Criteria 8. Buffers during plan review and construction. The limits and uses of the stream buffer systems should be well defined during each stage of the development process—from initial plan review, through construction.

Criteria 9: Buffer education and enforcement. The future integrity of a buffer system requires a strong education and enforcement program. Thus, it is important to make the buffer "visible" to the community, and to encourage greater buffer awareness and stewardship among adjacent residents. Several simple steps can be taken to accomplish this.

• Mark the buffer boundaries with permanent signs that describe allowable uses

• Educate buffer owners about the benefits and uses of the buffer with pamphlets, stream walks and meetings with homeowners associations

• Ensure that new owners are fully informed about buffer limits/uses when property is sold or transferred.

• Engage residents in a buffer stewardship program that includes reforestation and backyard "bufferscaping" programs

• Conduct annual buffer walks to check on encroachment

Criteria 10. Buffer flexibility. In most regions of the country, a hundred-foot buffer will take about 5% of the total land area in any given watershed out of use or production. While this constitutes a relatively modest land reserve at the watershed scale, it can be a significant hardship for a landowner whose property is adjacent to a stream. Many communities are legitimately concerned that stream buffer requirements could represent an uncompensated "taking" of private property. These concerns can be eliminated if a community incorporates several simple measures to ensure fairness and flexibility when administering its buffer program. As a general rule, the intent of the buffer program is to modify the *location* of development in relation to the stream but not its overall *intensity*. Some flexible measures in the buffer ordinance include:

• Maintaining buffers in private ownership

• Buffer averaging

• Density compensation

• Variances

• Conservation easements

kudzu will kill vegetation. Generally, forest species planted on agricultural land will eventually shade out pasture grasses and weeds, although some initial control (disking, mowing, burning) might be required to ensure tree establishment.

Plant Community Restoration

An objective of stream corridor restoration work might be to restore natural patterns of plant community distribution within the stream corridor. Numerous publications describe general distribution patterns for various geomorphic settings and flow conditions (e.g., Brinson et al. 1981, Wharton et al. 1982), and county soil surveys generally describe native vegetation for particular soils. More detailed and site-specific plant community descriptions may be available from state Natural Heritage programs, chapters of The Nature Conservancy, or other natural resources agencies and organizations.

Examination of the reference stream corridor, however, is often the best way to develop information on plant community composition and distribution. Once reference plant communities are defined, design can begin to detail the measures required to restore those communities (**Figure 8.10**). Rarely is it feasible or desirable to attempt to plant the full complement of appropriate species on a particular site. Rather, the more typical approach is to plant the dominant species or those species unlikely to colonize the site readily. For example, in the complex bottomland hardwood forests of the Southeast, the usual focus is on

planting oaks. Oaks are heavy-seeded, are often shade-intolerant, and may not be able to readily invade large areas for generations unless they are introduced in the initial planting plan, particularly if flooding has been reduced or curtailed. It is assumed that lighter-seeded and shade-tolerant species will invade the site at rates sufficient to ensure that the resulting forest is adequately diverse. This process can be accelerated by planting corridors of fast-growing species (e.g., cottonwoods) across the restoration area to promote seed dispersal.

Figure 8.9: Remnant vegetation and woody debris along a stream. *Attempts should be made to preserve existing vegetation within the stream corridor.*

Figure 8.10: A thriving and diverse plant community within a stream corridor. *Examination of reference plant communities is often the best way to develop information on the composition and distribution of plant communities at the restoration site.*

In areas typically dominated by cottonwoods and willows, the emphasis might be to emulate natural patterns of colonization by planting groves of particular species rather than mixed stands, and by staggering the planting program over a period of years to ensure structural variation. Where conifers tend to eventually succeed riparian hardwoods, some restoration designs may include scattered conifer plantings among blocks of pioneer species, to accelerate the transition to a conifer-dominated system.

Large-scale restoration work sometimes includes planting of understory species, particularly if they are required to meet specific objectives such as providing essential components of endangered species habitat. However, it is often difficult to establish understory species, which are typically not tolerant to full sun, if the restoration area is open. Where particular understory species are unlikely to establish themselves for many years, they can be introduced in adjacent forested sites, or planted after the initial tree plantings have matured sufficiently to

create appropriate understory conditions. This may also be an appropriate approach for introducing certain overstory species that might not survive planting in full sun (**Figure 8.11**)

The concept of focusing restoration actions on a limited group of overstory species to the exclusion of understory and other overstory species has been criticized. The rationale for favoring species such as oaks has been to ensure that restored riparian and floodplain areas do not become dominated by opportunistic species, and that wildlife functions and timber values associated with certain species will be present as soon as possible. It has been documented that heavy-seeded species such as oaks may be slow to invade a site unless planted (see *Tennessee Valley Authority Floodplain Reforestation Projects-50 Years Later*), but differential colonization rates probably exclude a variety of other species as well. Certainly, it would be desirable to introduce as wide a variety of appropriate species as possible; however, costs and the difficulties of doing supplemental plantings over a period of years might preclude this approach in most instances.

Plant species should be distributed within a restoration site with close attention to microsite conditions. In addition, if stream meandering behavior or scouring flows have been curtailed, special effort is required to maintain communities that normally depend on such behavior for natural establishment. These may include oxbow and swale communities (bald cypress, shrub wetlands, emergent

Figure 8.11: Restoration of understory plant species.

Understory species can be introduced at the restoration site after the initial tree plantings have matured sufficiently.

wetlands), as well as communities characteristic of newly deposited soils (cottonwoods, willows, alders, silver maple, etc.). It is important to recognize that planting vegetation on sites where regeneration mechanisms no longer operate is a temporary measure, and long-term management and periodic replanting is required to maintain those functions of the ecosystem.

In the past, stream corridor planting programs often included nonnative species selected for their rapid growth rates, soil binding characteristics, ability to produce abundant fruits for wildlife, or other perceived advantages over native species. These actions sometimes have unintended consequences and often prove to be ex-

Low Water Availability

In areas where water levels are low, artificial plantings will not survive if their roots cannot reach the zone of saturation. Low water availability was associated with low survival rates in more than 80 percent of unsuccessful revegetation work examined in Arizona (Briggs 1992). Planting long poles (20 ft) of Fremont cottonwood (*Populus fremontii*) and Gooding willow in augered holes has been successful where the ground water is more than 10 ft below the surface (Swenson and Mullins 1985). In combination with an irrigation system, many planted trees are able to reach ground water 10 ft below the surface when irrigated for two seasons after planting (Carothers et al. 1990). Sites closest to ground water, such as secondary channels, depressions, and low sites where water collects, are the best candidates for planting, although low-elevation sites are more prone to flooding and flood damage to the plantings. Additionally, the roots of many riparian species may become dormant or begin to die if inundated for extended periods of time (Burrows and Carr 1969).

tremely detrimental (Olson and Knopf 1986). As a result, many local, county, state, and federal agencies discourage or prohibit planting of nonnative species within wetlands or streamside buffers. Stream corridor restoration designs should emphasize native plant species from local sources. It may be feasible in some cases to focus restoration actions on encouraging the success of local seedfall to ensure that locally adapted populations of stream corridor vegetation are maintained on the site (Friedmann et al. 1995).

Plant establishment techniques vary greatly depending on site conditions and species characteristics. In arid regions, the emphasis has been on using poles or cuttings of species that sprout readily, and planting them to depths that will ensure contact with moist soil during the dry season (**Figure 8.12**). Where water tables have declined precipitously, deep auguring and temporary irrigation are used to establish cuttings and rooted or container-grown plants. In environments where precipitation or ground water is adequate to sustain planted vegetation, prolonged irrigation is less common, and bare-root or container-

Stream corridor restoration designs should emphasize native plant species from local sources.

Figure 8.12: Revegetation with the use of deeply planted live cuttings.
In arid regions, poles or cuttings of species that sprout readily are often planted to depths that assure contact with moist soil.

Tennessee Valley Authority Floodplain Reforestation Projects—50 Years Later

The oldest known large-scale restoration of forested wetlands in the United States was undertaken by the Tennessee Valley Authority in conjunction with reservoir construction projects in the south during the 1940s. Roads and railways were relocated outside the influence of maximum pool elevations, but where they were placed on embankments, TVA was concerned that they would be subject to wave erosion during periods of extreme high water. To reduce that possibility, agricultural fields between the reservoir and the embankments were planted with trees (**Figure 8.13**). At Kentucky Reservoir in Kentucky and Tennessee, approximately 1,000 acres were planted, mostly on hydric soils adjacent to tributaries of the Tennessee River. Detailed records were kept regarding the species planted and survival rates.

Figure 8.13: Kentucky Reservoir watershed, 1943.
Planting abandoned farmland with trees.

Some of these stands were recently located and studied to evaluate the effectiveness of the original reforestation effort, and to determine the extent to which the planted forests have come to resemble natural stands in the area.

Because the purpose of the plantings was erosion control, little thought was given to recreating natural patterns of plant community composition and structure. Trees were evenly spaced in rows, and planted species were apparently chosen for maximum flood tolerance. As a result, the studied stands had an initial composition dominated by bald cypress, green ash, red maple, and similarly water-tolerant species, but they did not originally contain many of the other common bottomland forest species, such as oaks.

Shear et al. (in press) compared the plant communities of the planted stands with forests on similar sites that had established by natural invasion of abandoned fields. They also looked at older stands that had never been converted to agriculture. The younger planted and natural stands were similar to the older stands with regard to understory composition, and measures of stand density and biomass were consistent with patterns typical for the age of the stands. Overstory composition of the planted stands was very different from that of the others, reflecting the original plantings. However, both the planted sites and the fields that had been naturally invaded had few individuals of heavy-seeded species (oaks and hickories), which made up 37 percent of the basal area of the older stands.

Oaks are an important component of southern bottomlands and are regarded as particularly important to wildlife. In most modern restoration plantings, oaks are favored on the assumption that they will not quickly invade agricultural fields. The stands at Kentucky Reservoir demonstrate that planted bottomland forests can develop structural and understory conditions that resemble those of natural stands within 50 years (**Figure 8.14**). Stands that established by natural invasion of agricultural fields had similar characteristics. The major compositional deficiency in both of the younger stands was the lack of heavy-seeded species. The results of this study appear to support the practice of favoring heavy-seeded species in bottomland forest restoration initiatives.

Figure 8.14: Kentucky Reservoir watershed in 1991.
Thriving bottomland hardwood forest.

grown plants are often used, particularly for species that do not sprout reliably from cuttings. On large floodplains of the South and East, direct seeding of acorns and planting of dormant bare-root material have been highly successful. Other options, such as transplanting of salvaged plants, have been tried with varying degrees of success. Local experience should be sought to determine the most reliable and efficient plant establishment approaches for particular areas and species, and to determine what problems to expect.

It is important to protect plantings from livestock, beaver, deer, small mammals, and insects during the establishment period. Mortality of vegetation from deer browsing is common and can be prevented by using tree shelters to protect seedlings.

Horizontal Diversity

Stream corridor vegetation, as viewed from the air, would appear as a mosaic of diverse plant communities that runs from the upland on one side of the stream corridor, down the valley slope, across the floodplain and up the opposite slope to the upland. With such broad dimensional range, there is a large potential for variation in vegetation. Some of the variation is a result of hydrology and stream dynamics, which will be discussed later in this chapter. Three important structural characteristics of horizontal diversity of vegetation are connectivity, gaps, and boundaries.

Connectivity and Gaps

As discussed earlier, *connectivity* is an important evaluation parameter of stream corridor functions, facilitating the processes of habitat, conduit, and filter/barrier. Stream corridor restoration design should maximize connections between ecosystem functions. Habitat and conduit functions can be enhanced by linking critical ecosystems to stream corridors through design that emphasizes orientation and proximity. Designers should consider functional connections to existing or potential features such as vacant or abandoned land, rare habitat, wetlands or meadows, diverse or unique vegetative communities, springs, ecologically innovative residential areas, movement corridors for flora and fauna, or associated stream systems. This allows for movement of materials and energy, thus increasing conduit functions and effectively increasing habitat through geographic proximity.

Generally, a long, wide stream corridor with contiguous vegetative cover is favored, though gaps are commonplace. The most fragile ecological functions determine the acceptable number and size of gaps. Wide gaps can be barriers to migration of smaller terrestrial fauna and indigenous plant species. Aquatic fauna may also be limited by the frequency or dimension of gaps. The width and frequency of gaps should therefore be designed in response to planned stream corridor functions. Bridges have been designed to allow migration of animals, along with physical and chemical connections of river and wetland flow. In Florida, for example, underpasses are constructed beneath roadways to serve as conduits for species movement (Smith and Hellmund 1993). The Netherlands has experimented with extensive species overpasses and

> **Restored plant communities should be designed to exhibit structural diversity and canopy closure similar to that of the reference stream corridor.**

underpasses to benefit particular species (**Figure 8.15**). Although not typically equal to the magnitude of an undisturbed stream corridor lacking gaps, these measures allow for modest functions as habitat and conduit.

The filtering capacity of stream corridors is affected by connectivity and gaps. For example, nutrient and water discharge flowing overland in sheet flow tends to concentrate and form rills. These rills in turn often form gullies. Gaps in vegetation offer no opportunity to slow overland flow or allow for infiltration. Where reference dimensions are similar and transferable, restored plant communities should be designed to exhibit structural diversity and canopy closure similar to that of the reference stream corridor. The reference stream corridor can provide information regarding plant species and their frequency and distribution. Design should aim to maintain the filtering capacity of the stream corridor by minimizing gaps in the corridor's width and length.

Buffer configuration and composition have also received attention since they influence wildlife habitat quality, including suitability as migration corridors for various species and suitability for nesting habitat. Reestablishment of linkages among elements of the landscape can be critically important for many species (Noss 1983, Harris 1984). However, as noted previously, fundamental considerations include whether a particular vegetation type has ever existed as a contiguous corridor in an area, and whether the predisturbance corridor was narrow or part of an expansive floodplain forest system. Establishment of inappropriate and narrow corridors can have a net detrimental influence at local and regional scales (Knopf et al. 1988). Local wildlife management priorities should be evaluated in developing buffer width criteria that address these issues.

Boundaries

The structure of the edge vegetation between a stream corridor and the adjacent landscape affects the habitat, conduit, and filter functions. A transition between two ecosystems in an undisturbed environment typically occurs across a broad area.

Boundaries between stream corridors and adjacent landscapes may be straight or curvilinear. A straight boundary allows relatively unimpeded movement along the edge, thereby decreasing species interaction between the two ecosystems. Conversely, a curvilinear boundary with lobes of the corridor and adjoining areas reaching into one another encourages movement across boundaries, resulting in increased interaction. The shape of the boundary can be designed to integrate or discourage these interactions, thus affecting the habitat, conduit, and filter functions.

Figure 8.15: Underpass design.

Underpasses should be designed to accommodate both vehicular traffic and movement of small fauna.
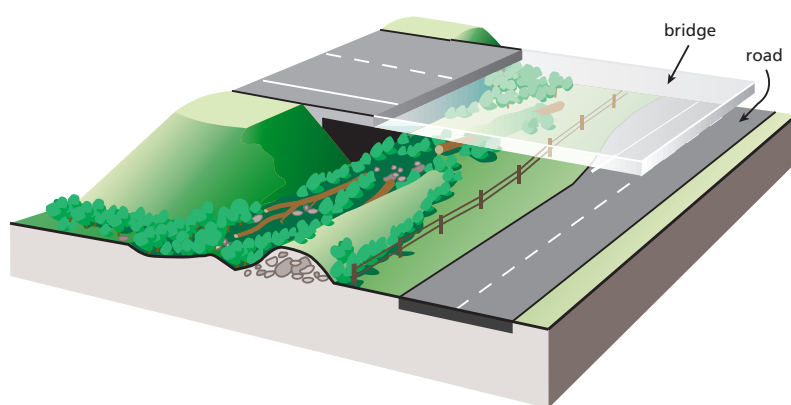
Species interaction may or may not be desirable depending on the project goals. The boundary of the restoration initiative can, for example, be designed to capture seeds or to integrate animals, including those carrying seeds. In some cases, however, this interaction is dictated by the functional requirements of the adjacent ecosystem (equipment tolerances within an agricultural field, for instance).

Vertical Diversity

Heterogeneity within the stream corridor is an important design consideration. The plants that make up the stream corridor, their form (herbs, shrubs, small trees, large trees), and their diversity affect function, especially at the reach and site scales. Stratification of vegetation affects wind, shading, avian diversity, and plant growth (Forman 1995). Typically, vegetation at the edge of the stream corridor is very different from the vegetation that occurs within the interior of the corridor. The topogra-

phy, aspect, soil, and hydrology of the corridor provide several naturally diverse layers and types of vegetation.

The difference between edge and interior vegetative structure are important design considerations (**Figure 8.16**). An edge that gradually changes from the stream corridor into the adjacent ecosystems will soften environmental gradients and minimize any associated disturbances. These transitional zones encourage species diversity and buffer variable nutrient and energy flows. Although human intervention has made edges more abrupt, the conditions of naturally occurring edge vegetation can be restored through design. The plant community and landform of a restored edge should reflect the structural variations found in the reference stream corridor. To maintain a connected and contiguous vegetative cover at the edge of small gaps, taller vegetation should be designed to continue through the gap. If the gap is wider than can be breached by the
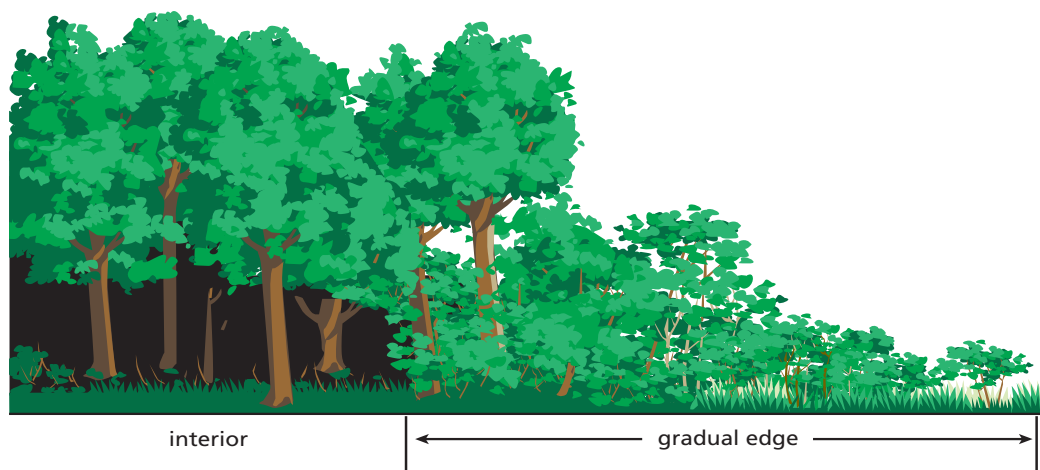

Figure 8.16: Edge vegetative structure.
Edge characteristics can be abrupt or gradual, with the gradual boundary typically encouraging more interaction between ecosystems.

interior   ◄──────── gradual edge ────────►

tallest or widest vegetation, a more gradual edge may be appropriate.

Vertical structure of the corridor interior tends to be less diverse than that of the edge. This is typically observed when entering a woodlot: edge vegetation is shrubby and difficult to traverse, whereas inner shaded conditions produce a more open forest floor that allows for easier movement. Snags and downed wood may also provide important habitat functions. When designing to restore interior conditions of stream corridor vegetation, a vegetation structure should be used that is less diverse than the vegetation structure used at the edge. The reference stream corridor will yield valuable information for this aspect of design.

Influence of Hydrology and Stream Dynamics

Natural floodplain plant communities derive their characteristic horizontal diversity primarily from the organizing influence of stream migration and flooding (Brinson et al. 1981). As discussed earlier, when designing restoration of stream corridor vegetation, nearby reference conditions are generally used as models to identify the appropriate plant species and communities. However, the original cover and older existing trees might have been established before stream regulation or other changes in the watershed that affect flow and sediment characteristics.

A good understanding of current and projected flooding is necessary for design of appropriately restored plant communities within the floodplain.

Water management and planning agencies are often the best sources of such data. In wildland areas, stream gauge data may be available, or on-site interpretation of landforms and vegetation may be required to determine whether floodplain hydrology has been altered through channel incision, beaver activity, or other causes. Discussions with local residents and examination of aerial photography may also provide information on water diversions, ground water depletion, and similar changes in the local hydrology.

A vegetation-hydroperiod model can be used to forecast riparian vegetation distribution (Malanson 1993). The model identifies the inundating discharges of various locations in the riparian zone and the resulting suitability of moisture conditions for desired plants. Grading plans, for example, can be adjusted to alter the area inundated by a given discharge and thus increase the area suitable for vegetation associated with a particular frequency and duration of flooding. A focus on the vegetation-hydroperiod relationship will demonstrate the following:

- The importance of moisture conditions in structuring vegetation of the riparian zone;

- The existence of reasonably well accepted physical models for calculating inundation from streamflow and the geometry of the bottomland.

- The likelihood that streamflow and inundating discharges have been altered in degraded stream systems or will be

modified as part of a restoration effort.

Generally, planting efforts will be easier when trying to restore vegetation on sites that have suitable moisture conditions for the desired vegetation, such as in replacing historical vegetation on cleared sites that have unaltered streamflow and inundating discharges. Moisture suitability calculations will support designs. Sometimes the restoration objective is to restore more of the desired vegetation than the new flow conditions would naturally support. Direct manipulation by planting and controlling competition can often produce the desired results within the physiological tolerances of the desired species. However, the vegetation on these sites will be out of balance with the site moisture conditions and might require continued maintenance. Management of vegetation can also accelerate succession to a more desirable state.

Projects that require long-term supplemental watering should be avoided due to high maintenance costs and decreased potential for success.   Inversely, there may be cases where the absence of vegetation, especially woody vegetation, is desired near the stream channel. Alteration of streamflow or inundating discharges might make moisture conditions on these sites unsuitable for woody vegetation.

The general concept of site suitability for plant species can be extended from moisture conditions determined by inundation to other variables determining plant distribution. For example, Anderson (1996) suggests that restoration of native riparian vegetation in arid southwestern river systems may be limited by unsuitable soil salinities. In many arid situations, depth to ground water might be a more direct measure of the moisture effects of streamflow on riparian sites than actual inundation. Both inundating discharge and depth to ground water are strongly related to elevation. However, depth to ground water may be the more appropriate causal variable for these rarely inundated sites, and a physical model expressing the dependence of alluvial ground water levels on streamflow might therefore be more important than a hydraulic model of surface water elevations.

Some stream corridor plant species have different requirements at different life stages. For example, plants tolerating extended inundation as adults may require a drawdown for establishment, and plants thriving on relatively high and dry sites as adults may be established only on moist surfaces near the water's edge. This can complicate what constitutes suitable moisture conditions and may require separate consideration of establishment requirements, and perhaps consideration of how sites might change over time. The application of simulation models of plant dynamics based on solving sets of explicit rules for how plant composition will change over time may become necessary as increasingly complex details of different requirements at different plant life history stages are incorporated into the evaluation of site suitability. Examples of this type of more sophisticated plant response model include Van der Valk (1981) for prairie marsh species and Pearlstine et al. (1985) for bottomland hardwood tree species.
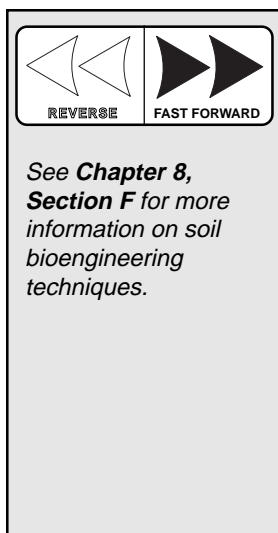
Soil bioengineering for floodplains and uplands

Soil bioengineering is the use of live and dead plant materials, in combination with natural and synthetic support materials, for slope stabilization, erosion reduction, and vegetative establishment.

There are many soil bioengineering systems, and selection of the appropriate system or systems is critical to successful restoration. Reference documents should be consulted to ensure that the principles of soil bioengineering are understood and applied. The *NRCS National Engineering Handbook, Part 650* (Chapter 16, Streambank and Shoreline Protection and Chapter 18, Soil Bioengineering for Upland Slope Protection and Erosion Reduction) offers background and guidelines for application of this technology. A more detailed description of soil bioengineering systems is offered in Section 8.F, Streambank Stabilization Design, of this chapter and in the Appendix A.

8.D. Habitat Measures

Other measures may be used to provide structure and functions. They may be implemented as separate actions or as an integral part of the restoration plan to improve habitat, in general, or for specific species. Such measures can provide short-term habitat until overall restoration results reach the level of maturity needed to provide the desired habitat. These measures can also provide habitat that is in short supply. Greentree reservoirs, nest structures, and food patches are three examples. Beaver are also presented as a restoration measure.

Greentree Reservoirs

Short-term flooding of bottomland hardwoods during the dormant period of tree growth enhances conditions for some species (e.g., waterfowl) to feed on mast and other understory food plants, like wild millet and smartweed. Acorns are a primary food source in stream corridors for a variety of fauna, including ducks, nongame birds and mammals, turkey, squirrel, and deer. Greentree reservoirs are shallow, forested floodplain impoundments usually created by building low levees and installing outlet structures (**Figure 8.17**). They are usually flooded in early fall and drained during late March to mid-April. Draining prevents damage to overstory hardwoods (Rudolph and Hunter 1964). Most existing greentree reservoirs are in the Southwest.

The flooding of greentree reservoirs, by design, differs from the natural flood regime. Greentree reservoirs are typically flooded earlier and at depths greater than would normally occur under natural conditions. Over time, modifications of natural flood conditions can result in vegetation changes, lack of regeneration, decreased mast production, tree mortality, and disease. Proper management of green tree reservoirs requires knowledge of the local system—especially the natural flood regime—and the integration of management goals that are consistent with system requirements. Proper management of greentree reservoirs can provide quality habitat on an annual basis, but the management plan must be well designed from construction through management for waterfowl.

Nest Structures

Loss of riparian or terrestrial habitat in stream corridors has resulted in the decline of many species of birds and

Figure 8.17: Bottomland hardwoods serving as a greentree reservoir.
Proper management of greentree reservoirs requires knowledge of the local system.

mammals that use associated trees and tree cavities for nesting or roosting. The most important limiting factor for cavity-nesting birds is usually the availability of nesting substrate (von Haartman 1957), generally in the form of snags or dead limbs in live trees (Sedgwick and Knopf 1986). Snags for nest structures can be created using explosives, girdling, or topping of trees. Artificial nest structures can compensate for a lack of natural sites in otherwise suitable habitat since many species of birds will readily use nest boxes or other artificial structures. For example, along the Mississippi River in Illinois and Wisconsin, where nest trees have become scarce, artificial nest structures have been erected and constructed for double-crested cormorants using utility poles (Yoakum et al. 1980). In many cases, increases in breeding bird density have resulted from providing such structures (Strange et al. 1971, Brush 1983). Artificial nest structures can also improve nestling survival (Cowan 1959).

Nest structures must be properly designed and placed, meeting the biological needs of the target species. They should also be durable, predator-proof, and economical to build. Design specifications for nest boxes include hole diameter and shape, internal box volume, distance from the floor of the box to the opening, type of material used, whether an internal "ladder" is necessary, height of placement, and habitat type in which to place the box. Other types of nest structures include nest platforms for waterfowl and raptors; nest baskets for doves, owls, and waterfowl; floating

nest structures for geese; and tire nests for squirrels. Specifications for nest structures for riparian and wetland nesting species (including numerous Picids, passerines, waterfowl, and raptors) can be found in many sources including Yoakum et al. (1980), Kalmbach et al. (1969), Payne (1992), and various state wildlife agency and conservation publications.

Food Patches

Food patch planting is often expensive and not always predictable, but it can be carried out in wetlands or riparian systems mostly for the benefit of waterfowl. Environmental requirements of the food plants native to the area, proper time of year of introduction, management of water levels, and soil types must all be taken into consideration. Some of the more important food plants in wetlands include pondweed (*Potamogeton* spp.), smartweed (*Polygonum* spp.), duck potato, spike sedges (*Carex* spp.), duckweeds (*Lemna* spp.), coontail, alkali bulrush (*Scirpus paludosus*), and various grasses. Two commonly planted native species include wild rice (*Zizania*) and wild millet. Details on suggested techniques for planting these species can be found in Yoakum et al. (1980).

Importance of Beaver to Riparian Ecosystems

Beaver have long been recognized for their potential to influence riparian systems. In rangelands, where loss of riparian functional value has been most dramatic, the potential role of beaver in restoring degraded streams is least understood.

Beaver dams on headwater streams can positively influence riparian function in many ways, as summarized by Olson and Hubert (1994) (**Figure 8.18**). They improve water quality by trapping sediments behind dams and by reducing stream velocity, thereby reducing bank erosion (Parker 1986). Beaver ponds can alter water chemistry by changing adsorption rates for nitrogen and phosphorus (Maret 1985) and by trapping coliform bacteria (Skinner et al. 1984). The flow regime within a watershed can also be influenced by beaver. Beaver ponds create a sponge-like effect by increasing the area where soil and water meet (**Figure 8.19**). Headwaters retain more water from spring runoff and major storm events, which is released more slowly, resulting in a higher water table and extended summer flows. This increase in water availability, both surface and subsurface, usually increases the width of the riparian zone and, consequently, favors wildlife communities that depend on that vegetation. There can be negative impacts as well, including loss of spawning habitat, increase in water temperatures beyond optimal levels for some fish species, and loss of riparian habitat.

Richness, diversity, and abundance of birds, herpetiles, and mammals can be increased by the activities of beaver (Baker et al. 1992; Medin and Clary 1990). Beaver ponds are important waterfowl production areas and can also be used during migration (Call 1970, Ringelman 1991). In some high-elevation areas of the Rocky Mountains, beaver are solely responsible for the majority of local duck production. In addition, species of high interest, such as trumpeter swans, sandhill cranes, moose, mink, and river otters, use beaver ponds for nesting or feeding areas (Collins 1976).

Transplanting Beaver to Restore Stream Functions

Beaver have been successfully transplanted into many watersheds throughout the United States during the past 50 years. This practice was very common during the 1950s after biologists realized the loss of ecological function resulting from overtrapping of beaver by fur traders before the turn of the century. Reintroduction of beaver has restored the U.S. beaver population to 6-12 million, compared to a pre-European level of 60-400 million (Naiman et al. 1986). Much unoccupied habitat or potential habitat still remains, especially in the shrub-steppe ecosystem.

Figure 8.18: Beaver dam on a headwater stream.
Beavers have many positive impacts on headwater streams.

Figure 8.19: A beaver pond.
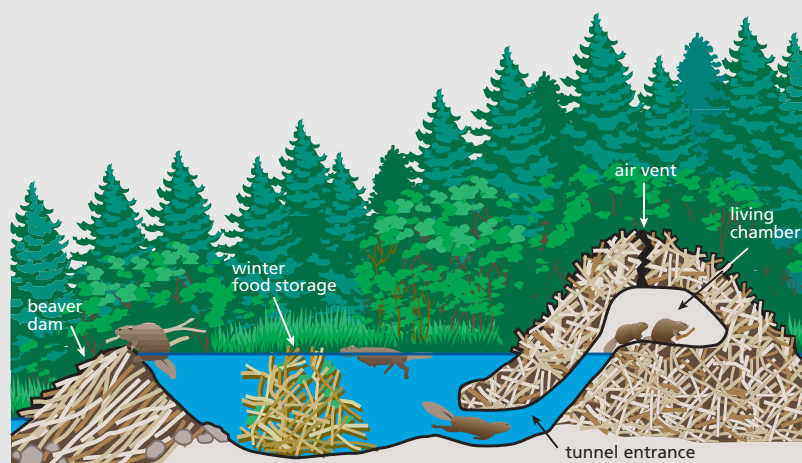*Beaver ponds create a sponge-like effect.*

Figure 8.20: Beaver habitat.
It is advisable to obtain beaver from habitat that is similar to where they will be introduced.

Figure 8.21: A beaver lodge.

The living chamber in a beaver lodge is above water and used year-round. Deep entrances enable beavers to obtain food from underwater caches in winter.

In forested areas, where good beaver habitat already exists, reintroduction techniques are well established. The first question asked should be "If the habitat is suitable, why are beaver absent?" In the case of newly restored habitat or areas far from existing populations, reintroduction without habitat improvement might be warranted (**Figure 8.20**). Beavers are livetrapped from areas that have excess populations or from areas where they are a nuisance. It is advisable to obtain beavers from habitat that is similar to where they will be introduced to ensure they are familiar with available food and building materials (Smith and Prichard 1992). This is particularly important in shrub-steppe habitats.

Reintroduction into degraded riparian areas within the shrub-steppe zone is controversial. Conventional wisdom holds that a yearlong food supply must be present before introducing beaver. In colder climates, this means plants with edible bark, such as willow, cottonwood, or aspen, must be present to provide a winter food supply for beaver (**Figure 8.21**). But often these species are the goal of restoration. In some cases willows or other species can be successfully planted as described in other sections of this document. In other areas, conditions needed to sustain planted cuttings, such as a high water table and minimal competition with other vegetation, might preclude successful establishment. Transplanting beaver before willows are established may create the conditions needed to both establish and maintain riparian shrubs or trees. In these cases it may be helpful to provide beaver with a pickup truck load of aspen or other trees to use as building material at or near the reintroduction site. This may encourage beaver to stay near the site and strengthen dams built of sagebrush or other shrubs (Apple et al. 1985).

Nuisance Beaver

Unfortunately, beaver are not beneficial in all situations, which is all too obvious to those managing damage control. In many cases where they live in close proximity to humans or features important to humans, beaver need to be removed or their damage controlled. Common problems include cutting or eating desirable vegetation, flooding roads or irrigation ditches by plugging culverts, and increasing erosion by burrowing into the banks of streams or reservoirs. In addition, beaver carry *Giardia* species pathogens, which can infect drinking water supplies and cause human health problems.

Control of nuisance beaver usually involves removing the problem animals directly or modifying their habitat. Beaver can be livetrapped (Bailey or Hancock traps) and relocated to a more acceptable location or killed by dead-traps (e.g., Conibear #330) or shooting (Miller 1983). In cases where the water level in a dam must be controlled to prevent flooding, a pipe can be placed through the dam with the upstream side perforated to allow water flow.

8.E Stream Channel Restoration

Some disturbances to stream channels (e.g., from surface mining activities, extreme weather events, or major highway construction) are so severe that restoration within a desired time frame requires total reconstruction of a new channel. Selecting dimensions (width, depth, cross-sectional shape, pattern, slope, and alignment) for such a reconstructed channel is perhaps the most difficult component of stream restoration design. In the case of stream channel reconstruction, stream corridor restoration design can proceed along one of two broad tracks:

1. *A single-species restoration that focuses on habitat requirements of certain life stages of species (for example, rainbow trout spawning).* The existing system is analyzed in light of what is needed to provide a given quantity of acceptable habitat for the target species and life stage, and design proceeds to remedy any deficiencies noted.

2. *An "ecosystem restoration" or "ecosystem management" approach that focuses design resources on the chemical, hydrologic, and geomorphic functions of the stream corridor.* This approach assumes that communities will recover to a sustainable level if the stream corridor structure and functions are adequate. The strength of this approach is that it recognizes the complex interdependence between living things and the totality of their environments.

Although methods for single-species restoration design pertaining to treatments for aquatic habitat are included elsewhere in this chapter, the second track is emphasized in this section.

Procedures for Channel Reconstruction

If watershed land use changes or other factors have caused changes in sediment yield or hydrology, restoration to an historic channel condition is not recommended. In such cases, a new channel design is needed. The following procedures are suggested:

1. *Describe physical aspects of the watershed and characterize its hydrologic response.*

   This step should be based on data collected during the planning phase, as described in Chapter 4.

2. *Considering reach and associated constraints, select a preliminary right-of-way for the restored stream channel corridor and compute the valley length and valley slope.*

3. *Determine the approximate bed material size distribution for the new channel.*

Many of the channel design procedures described below require the designer to supply the size of bed sediments. If the project is not likely to modify bed sediments, the existing channel bed may be sampled using

Review Chap 4's data collection planning section.
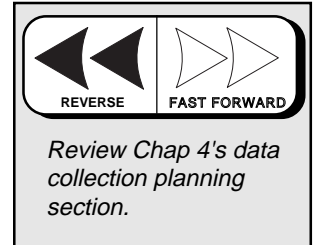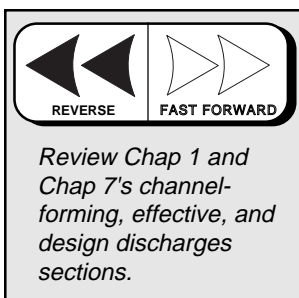
procedures reviewed in Chapter 7. If predisturbance conditions were different from those of the existing channel, and if those conditions must be restored, the associated sediment size distribution must be determined. This can be done by collecting representative samples of bed sediments from nearby, similar streams; by excavating to locate the predisturbance bed; or by obtaining the information from historic resources.

Like velocity and depth, bed sediment size in natural streams varies continuously in time and space. Particularly troublesome are streams with sediment size distributions that are bimodal mixtures of sand and gravel, for example. The median (D_{50}) of the overall distribution might be virtually absent from the bed. However, if flow conditions allow development of a well-defined armor layer, it might be appropriate to use a higher percentile than the median (e.g., the D_{75}) to represent the bed material size distribution. In some cases, a new channel excavated into a heterogeneous mixture of noncohesive material will develop an armor layer. In such a case, the designer must predict the likely size of the armor layer material. Methods presented by Helwig (1987) and Griffiths (1981) could prove helpful in such a situation.

4. *Conduct a hydrologic and hydraulic analysis to select a design discharge or range of discharges.*

Conventional channel design has revolved around selecting channel dimensions that convey a certain discharge at or below a certain elevation. Design discharge is usually

based on flood frequency or duration or, in the case of canals, on downstream supply needs. Channel restoration, on the other hand, implies designing a channel similar to one that would develop naturally under similar watershed conditions.

Therefore, the first step in selecting a design discharge for restoration is not to determine the controlling elevation for flood protection but to determine what discharge controls channel size. Often this will be at or close to the 1- to 3-year recurrence interval flow. See Chapters 1 and 7 for discussions of channel-forming, effective, and design discharges. Additional guidance regarding streamflow analysis for gauged and ungauged sites is presented in Chapter 7. The designer should, as appropriate to the stream system, compute effective discharge or estimate bankfull discharge.

A sediment rating curve must be developed to integrate with the flow duration curve to determine the effective discharge. The sediment load that is responsible for shaping the channel (bed material load) should be used in the calculation of the effective discharge. This sediment load can be determined from measured data or computed using an appropriate sediment transport equation. If measured suspended sediment data are used, the wash load, typically consisting of particles less than 0.062 mm, should be deleted and only the suspended bed material portion of the suspended load used. If the bed load in the stream is considered to be only a small percentage of the total bed material load, it might be acceptable to simply use the measured suspended bed material load in the effective discharge calculations.

However, if the bed load is a significant portion of the load, it should be calculated using an appropriate sediment transport function and then added to the suspended bed material load to provide an estimate of the total bed material load. If bed load measurements are available, which seldom is the case, these observed data can be used.

Flow levels and frequencies that cause flooding also need to be identified to help plan and design out-of-stream restoration measures in the rest of the stream corridor. If flood management is a constraint, additional factors that are beyond the scope of this document enter the design. Environmental features for flood control channels are described elsewhere (Hey 1995, Shields and Aziz 1992, USACE 1989a, Brookes 1988).

Channel reconstruction and stream corridor restoration are most difficult for incised streams, and hydrologic analyses must consider several additional factors. Incised stream channels are typically much larger than required to convey the channel-forming discharge. Restoration of an incised channel may involve raising the bottom of a stream to restore overbank flow and ecological functions of the floodplain. In this type of restoration, compatibility of restored floodplain hydrology with existing land uses must be considered.

A second option in reconstructing incised channels is to excavate one or both sides to create a new bankfull channel with a floodplain (Hey 1995). Again, adjacent land uses must be able to accommodate the new, excavated floodplain/channel.

A third option is to stabilize the incised channel in place, and to enhance the low-flow channel for environmental benefits. The creation of a floodplain might not be necessary or possible as part of a stream restoration.

In cases where channel sizing, modification, or realignment are necessary, or where structures are required to enhance vertical or lateral stability, it is critical that restoration design also include consideration of the range of flows expected in the future. In urbanizing watersheds, future conditions may be quite different from existing conditions, with higher, sharper, peak flows.

If certain instream flow levels are required to meet restoration objectives, it is imperative that those flows be quantified on the basis of a thorough understanding of present and desired conditions. Good design practice also requires checking stream channel hydraulics and stability at discharges well above and below the design condition. Stability checks (described below) may be quite simple or very sophisticated. Additional guidance on hydrologic analysis and development of stage-discharge relationships are presented in Chapter 7.

5. *Predict stable planform type (straight, meandering, or braided).*

Channel planform may be classified as straight, braided, or meandering, but thresholds between categories are arbitrary since channel form can vary continuously from straight to single-channel meanders to multiple braids. Naturally straight, stable alluvial channels are rare, but meandering and braided channels are common and can
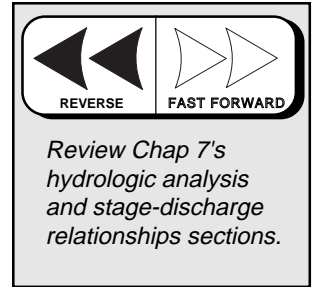
display a wide range of lateral and vertical stability.

Relationships have been proposed that allow prediction of channel planform based on channel slope, discharge, and bed material size (e.g., Chang 1988), but they are sometimes unreliable (Chitale 1973, Richards 1982) and give widely varying estimates of the slope threshold between meandering and braiding. As noted by Dunne (1988), "The planform aspects of rivers are the most difficult to predict," a sentiment echoed by USACE (1994), "... available analytical techniques cannot determine reliably whether a given channel modification will be liable to meander development, which is sensitive to difficult-to-quantify factors like bank vegetation and cohesion."

Stable channel bed slope is influenced by a number of factors, including sediment load and bank resistance to erosion. For the first iteration, restoration designers may assume a channel planform similar to stable reference channels in similar watersheds. By collecting data for stable channels and their valleys in reference reaches, insight can be gained on what the stable configuration would be for the restoration area. The morphology of those stream types can also provide guidance or additional converging lines of evidence that the planform selected by the designer is appropriate.

After initial completion of these five steps, any one of several different paths may be taken to final design. Three approaches are summarized in **Table 8.1**. The tasks are not always executed sequentially because trial and error and reiteration are often needed.

Alignment and Average Slope

In some cases, it might be desirable to divert a straightened stream into a meandering alignment for restoration purposes. Five approaches for meander design are summarized in the adjacent box.

For cases where the design channel will carry only a small amount of bed material load, bed slope and channel dimensions may be selected to carry the design discharge at a velocity that will be great enough to prevent suspended sediment deposition and small enough to prevent erosion of the bed. This approach is suitable only for channels with beds that are stationary or move very infrequently—typically stable cobble- and gravel-bed streams.

Once mean channel slope is known, channel length can be computed by multiplying the straight line down-valley distance by the ratio of valley slope to channel slope (sinuosity). Meanders can then be laid out using a piece of string on a map or an equivalent procedure, such that the meander arc length L (the distance between inflection points, measured along the channel) ranges from 4 to 9 channel widths and averages 7 channel widths. Meanders should not be uniform.

The incised, straightened channel of the River Blackwater (Norfolk, United Kingdom) was restored to a meandering form by excavating a new low-level floodplain about 50 to 65 feet wide containing a sinuous channel about 16 feet wide and 3 feet deep (Hey 1995). Preliminary calculations indicated that the bed of the channel was only slightly mobile at bankfull discharge, and sediment loads were

Table 8.1: Three approaches to achieving final design.

There are variations of the final steps to a restoration design, after the first five steps described in the text are done.

Approach A		Approach B (Hey 1994)		Approach C (Fogg 1995)	
Task	Tools	Task	Tools	Task	Tools
Determine meander geometry and channel alignment[1].	Empirical formulas for meander wavelength, and adaptation of measurements from predisturbed conditions or nearly undisturbed reaches.	Determine bed material discharge to be carried by design channel at design discharge, compute bed material sediment concentration.	Analyze measured data or use appropriate sediment transport function[2] and hydraulic properties of reach upstream from design reach.	Compute mean flow, width, depth, and slope at design discharge.[4]	Regime or hydraulic geometry formulas with regional coefficients.
Compute sinuosity, channel length, and slope.	Channel length = sinuosity X valley length. Channel slope= valley slope/ sinuosity.	Compute mean flow, width, depth, and slope at design discharge.[4]	Regime or hydraulic geometry formulas with regional coefficients, or analytical methods (e.g. White, et.al., 1982, or Copeland, 1994)[3].	Compute or estimate flow resistance coefficient at design discharge.	Appropriate relationship between depth, bed sediment size, and resistance coefficient, modified based on expected sinuosity and bank/berm vegetation.
Compute mean flow width and depth at design discharge.[4]	Regime or hydraulic geometry formulas with regional coefficients, and resistance equations or analytical methods (e.g. tractive stress, Ikeda and Izumi, 1990, or Chang, 1988).	Compute sinuosity and channel length.	Sinuosity = valley slope/ channel slope. Channel length= sinuosity X valley length.	Compute mean channel slope and depth required to pass design discharge.	Uniform flow equation (e.g. Manning, Chezy) continuity equation, and design channel cross-sectional shape; numerical water surface profile models may be used instead of uniform flow equation.
Compute riffle spacing (if gravel bed), and add detail to design.	Empirical formulas, observation of similar streams, habitat criteria.	Determine meander geometry and channel alignment.	Lay out a piece of string scaled to channel length on a map (or equivalent procedure) such that meander arc lengths vary from 4 to 9 channel widths.	Compute velocity or boundary sheer stress at design discharge.	Allowable velocity or shear stress criteria based on channel boundary materials
Check channel stability and reiterate as needed.	Check stability.	Compute riffle spacing (if gravel bed), and add detail to design.	Empirical formulas, observation of similar streams, habitat criteria.	Compute sinuosity and channel length.	Sinuosity = valley slope/ channel slope. Channel length= sinuosity X valley length.
		Check channel stability and reiterate as needed.	Check stability.	Compute sinuosity and channel length.	Lay out a piece of string scaled to channel length on a map (or equivalent procedure) such that meander arc lengths vary from 4 to 9 channel widths.
				Check channel stability and reiterate as needed.	Check stability.

[1] Assumes meandering planform would be stable. Sinuosity and arc-length are known.

[2] Computation of sediment transport without calibration against measured data may give highly unreliable results for a specific channel (USACE, 1994, Kuhnle, et.al., 1989).

[3] The two methods listed assume a straight channel. Adjustments would be needed to allow for effects of bends.

[4] Mean flow width and depth at design discharge will give channel dimensions since design discharge is bankfull. In some situation channel may be increased to allow for freeboard. Regime and hydraulic geometry formulas should be examined to determine if they are mean width or top width.

A systematic design methodology has been developed for use in designing restoration projects that involve channel reconstruction (USACE, WES). The methodology includes use of hydraulic geometry relationships, analytical determination of stable channel dimensions, and a sediment impact assessment. The preferred geometry is a compound channel with a primary channel designed to carry the effective or "channel forming" discharge and an overbank area designed to carry the additional flow for a specified flood discharge. Channel width may be determined by analogy methods, hydraulic geometry predictors, or analytically. Currently under development are hydraulic geometry predictors for various stream types. Once a width is determined for the effective discharge, depth and channel slope are determined analytically by balancing sediment inflow from upstream with sediment transport capacity through the restored channel. Meander wavelength is determined by analogy or hydraulic geometry relationships. Assumption of a sine-generated curve then allows calculation of channel planform. The stability of the channel design is then evaluated for the full range of expected discharges by conducting a sediment impact assessment. Refinements to the design include variation of channel widths at crossings and pools, variable lateral depths in pools, coarsening of the channel bed in riffles, and bank protection.

low. A carbon copy design process was used, recreating meander geometry from the mid-19th century (Hey 1994). The River Neath (Wales, United Kingdom), an active gravel-bed stream, was diverted at five locations into meandering alignments to allow highway construction. Existing slopes were maintained through each diversion, effectively illustrating a "slope-first" design (Hey 1994).

Channel Dimensions

Selection of channel dimensions involves determining average values for width and depth. These determinations are based on the imposed water and sediment discharge, bed sediment size, bank vegetation, resistance, and average bed slope. However, both width and depth may be constrained by site factors, which the designer must consider once stability criteria are met. Channel width must be less than the available corridor width, while depth is dependent on the upstream and downstream controlling elevations, resistance, and the elevation of the adjacent ground surface. In some cases, levees or floodwalls might be needed to match site constraints and depth requirements. Average dimensions determined in this step should not be applied uniformly. Instead, in the detailed design step described below, nonuniform slopes and cross sections should be specified to create converging and diverging flow and resulting physical diversity.

The average cross-sectional shape of natural channels is dependent on discharge, sediment inflow, geology, roughness, bed slope, bank vegetation, and bed and bank materials. Although bank vegetation is considered when using some of the empirical tools presented below, many of the analytical approaches do not consider the influence of bank material and vegetation or make unrealistic assumptions (e.g., banks are composed of the same material as the bed). These tools should be used with care. After initial selection of average channel width and depth, designers should consider the compatibility of these dimensions with reference reaches.

Reference Reaches

Perhaps the simplest approach to selecting channel width and depth is to use dimensions from stable reaches elsewhere in the watershed or from similar reaches in the region. The difficulty in this approach is finding a suitable reference reach. A reference reach is a reach of stream outside the project reach that is used to develop design criteria for the project reach.
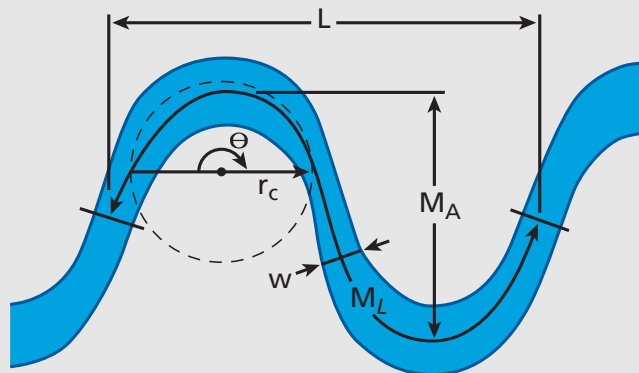
A reference reach used for stable channel design should be evaluated to make sure that it is stable and has a desirable morphological and ecological condition. In addition, the reference reach must be similar enough to the desired project reach so that the comparison is valid. It must be similar to the desired project reach in hydrology, sediment load, and bed and bank material.

The term *reference reach* has several meanings. As used above, the reference reach is a reach that will be used as a template for the geometry of the restored channel. The width, depth, slope, and planform characteristics of the reference reach are transferred to the design reach, either exactly or by

Meander Design

Five approaches to meander design are described below, not in any intended order of priority. The first four approaches result in average channel slope being determined by meander geometry. These approaches are based on the assumption that the controlling factors in the stream channel (water and sediment inputs, bed material gradation, and bank erosional resistance) will be similar to those in the reference reach (either the restoration reach before disturbance or undisturbed reaches). The fifth approach requires determination of stream channel slope first. Sinuosity follows as the ratio of channel slope to valley slope, and meander geometry (**Figure 8.22**) is developed to obtain the desired sinuosity.

1. **Replacement of meanders exactly as found before disturbance (the carbon copy technique).** This method is appropriate if hydrology and bed materials are very similar or identical to predisturbance conditions. Old channels are often filled with cohesive soils and may have cohesive boundaries. Accordingly, channel stability may be enhanced by following a previous channel alignment.

2. **Use of empirical relationships that allow computation of meander wavelength, *L*, and amplitude based on channel width or discharge.** Chang (1988) presents graphical and algebraic relationships between meander wavelength, width-depth ratio, and friction factor. In addition to meander wavelength, specification of channel alignment requires meander radius of curvature (Hey 1976) and meander amplitude or channel slope. Hey (1976) also suggests that *L* is not usually uniquely determined by channel width or discharge. Rechard and Schaefer (1984) provide an example of development of regional formulas for meander restoration design. Chapter 7 includes a number of meander geometry relationships developed from regional data sets. Newbury and Gaboury (1993) designed meanders for a straightened stream (North Pine River) by selecting meander amplitude to fit between floodplain terraces. Meander wavelength was set at 12.4 times the channel width (on the high end of the literature range), and radius of curvature ranged from 1.9 to 2.3 times the channel width.

Figure 8.22: Variables used to describe and design meanders.
Consistent, clear terminology is used in meander design.
Adapted from Williams 1986.

L   meander wavelength
M_L meander arc length
w   average width at bankfull discharge
M_L meander amplitude
r_c radius of curvature
$\ominus$ arc angle

3. **Basin-wide analysis to determine fundamental wavelength, mean radius of curvature, and meander belt width in areas "reasonably free of geologic control."** This approach has been used for reconstruction of streams destroyed by surface mining in subhumid watersheds of the western United States. Fourier analysis may be used with data digitized from maps to determine fundamental meander wavelength (Hasfurther 1985).

4. **Use of undisturbed reaches as design models**. If the reach targeted for restoration is closely bounded by undisturbed meanders, dimensions of these undisturbed reaches may be studied for use in the restored reach (**Figure 8.23**). Hunt and Graham (1975) describe successful use of undisturbed reaches as models for design and construction of two meanders as part of river relocation for highway construction in Montana. Brookes (1990) describes restoration of the Elbaek in Denmark using channel width, depth, and slope from a "natural" reach downstream, confirmed by dimensions of a river in a neighboring watershed with similar area, geology, and land use.

5. **Slope first.** Hey (1994) suggests that meanders should be designed by first selecting a mean channel slope based on hydraulic geometry formulas. However, correlation coefficients for regime slope formulas are always much smaller than those for width or depth formulas, indicating that the former are less accurate. Channel slope may also be determined by computing the value required to convey the design water and sediment discharges (White et al. 1982, Copeland 1994). The main weakness of this approach is that bed material sediment discharge is required by analytical techniques and in some cases (e.g., Hey and Thorne 1986) by hydraulic geometry formulas. Sediment discharges computed without measured data for calibration may be unreliable.

Site-specific bed material samples and channel geometries are needed to apply these analytical techniques and to achieve confidence in the resulting design.

Figure 8.23: The natural meander of a stream.

Rivers meander to increase length and reduce gradient. Stream restorations often attempt to reconstruct the channel to a previous meandering condition or one "copied" from a reference reach.

using analytical or empirical techniques to scale them to fit slightly different characteristics of the project reach (for example, a larger or smaller drainage area).

It is impossible to find an exact replica of the watershed in which the restoration work is located, and subjective judgement may play a role in determining what constitutes similarity. The level of uncertainty involved may be reduced by considering a large number of stable reaches. By classifying the reference streams, width and depth data can be grouped by stream type to reduce the scatter inherent in regional analyses.

A second common meaning of the term *reference reach* is a reach with a desired biological condition, which will be used as a target to strive for when comparing various restoration options. For instance, for a stream in an urbanized area, a stream with a similar drainage area in a nearby unimpacted watershed might be used as a reference reach to show what type of aquatic and riparian community might be possible in the project reach. Although it might not be possible to return the urban stream to predevelopment conditions, the characteristics of the reference reach can be used to indicate what direction to move toward. In this use of the term, a reference reach defines desired biological and ecological conditions, rather than stable channel geometry. Modeling tools such as IFIM and RCHARC (see Chapter 7) can be used to determine what restoration options come closest to replicating the habitat conditions of the reference reach (although none of the options may exactly match it).

Application of Regime and Hydraulic Geometry Approaches

Typical regime and hydraulic geometry relationships are presented in Chapter 7. These formulas are most reliable for width, less reliable for depth, and least reliable for slope.

Exponents and coefficients for hydraulic geometry formulas are usually determined from data for the same stream, the same watershed, streams of a similar type, or the same physiographic region. Because formula coefficients vary, application of a given set of hydraulic geometry or regime relationships should be limited to channels similar to the calibration sites. Classifying streams can be useful in refining regime relationships (See Chapter 7's section on *Stream Classification*).

Published hydraulic geometry relationships are usually based on stable, single-thread alluvial channels. Hydraulic geometry relationships determined through stream classification of reference reaches can also be valuable for designing the stream restoration. Channel geometry-discharge relationships are more complex for multithread channels. Individual threads may fit the relationships if their partial bankfull discharges are used in place of the total streamflow. Also, hydraulic geometry relationships for gravel-bed rivers are far more numerous in the literature than those for sand-bed rivers.

A trial set of channel properties (average width, depth, and slope) can be evaluated by using several sets of regime and hydraulic geometry formulas and comparing results. Greatest weight should be given to formulas

based on sites similar to the project reach. A logical second step is to use several discharge levels in the best-suited sets of formulas. Because hydraulic geometry relationships are most compatible with single-channel sand and gravel streams with low bed-material sediment discharge, unstable channels (aggrading or degrading profiles) can depart strongly from published relationships.

Literature references to the use of hydraulic geometry formulas for sizing restored channels are abundant. Initial estimates for width and depth for the restored channel of Seminary Creek, which drains an urban water-shed in Oakland, California, were determined using regional hydraulic geometry formulas (Riley and MacDonald 1995). Hey (1994, 1995) discusses use of hydraulic geometry relationships determined using regres-sion analyses of data from gravel bed rivers in the United Kingdom for restoration design. Newbury and Gaboury (1993) used regional hydrau-lic geometry relations based on drain-age area to check width and depth of restored channels in Manitoba.

Hydraulic geometry formulas for sizing stream channels in restoration efforts must be used with caution since a number of pitfalls are associ-ated with their use:

- The formulas represent hy-draulic geometry only at bankfull or mean annual discharge. Designers must also select a single statistic to describe bed sediment size when using hydraulic geom-etry relationships. (However, refinements to the Hey and Thorne [1986] formulas for slope in Table 7.5 should be noted.)

- Downstream hydraulic geom-etry formulas are usually based on the bankfull discharge, the elevation of which can be extremely difficult to identify in vertically unstable channels.

- Exponents and coefficients selected for design must be based on streams with slopes, bed sediments, and bank materials similar to the one being designed.

- The premise is that the channel shape is dependent on only one or two variables.

- Hydraulic geometry relation-ships are power functions with a fair degree of scatter that may prove too great for reliable engineering design. This scatter is indicative of natural variability and the influence of other variables on channel geometry.

In summary, hydraulic geometry relationships are useful for preliminary or trial selection of design channel properties. Hydraulic and sediment transport analyses are recommended for final design for the restoration.

Analytical Approaches for Channel Dimensions

Analytical approaches for designing stream channels are based on the idea that a channel system may be de-scribed by a finite number of variables. In most practical design problems, a few variables are determined by site conditions (e.g., valley slope and bed material size), leaving up to nine

variables to be computed. However, designers have only three governing equations available: continuity, flow resistance (such as Manning, Chezy, and Darcy-Weisbach), and sediment transport (such as Ackers-White, Einstein, and Brownlie). Since this leaves more unknowns than there are equations, the system is indeterminate. Indeterminacy of the stable channel design problem has been addressed in the following ways:

- Using empirical relationships to compute some of the unknowns (e.g., meander parameters).

- Assuming values for one or more of the unknown variables.

- Using structural controls to hold one or more unknowns constant (e.g., controlling width with bank revetments).

- Ignoring some unknown variables by simplifying the channel system. For example, a single sediment size is sometimes used to describe all boundaries, and a single depth is used to describe water depth rather than mean and maximum depth as suggested by Hey (1988).

- Adopting additional governing equations based on assumed properties of streams with movable beds and banks. The design methods based on "extremal hypotheses" fall into this category. These approaches are discussed below under analytical approaches for channels with moving beds.

Table 8.2 lists six examples of analytical design procedures for sand-bed and gravel channels. These procedures are data-intensive and would be used in high-risk or large-scale channel reconstruction work.

Tractive Stress (No Bed Movement)

Tractive stress or tractive force analysis is based on the idea that by assuming negligible bed material discharge ($Q_s = 0$) and a straight, prismatic channel with a specified cross-sectional shape, the inequality in variables and governing equations mentioned above is eliminated. Details are provided in many textbooks that deal with stable channel design (e.g., Richards 1982, Simons and Senturk 1977, French 1985). Because the method is based on the laws of physics, it is less empirical and region-specific than regime or hydraulic

Review Chap. 7's section on hydraulic geometry relationships.
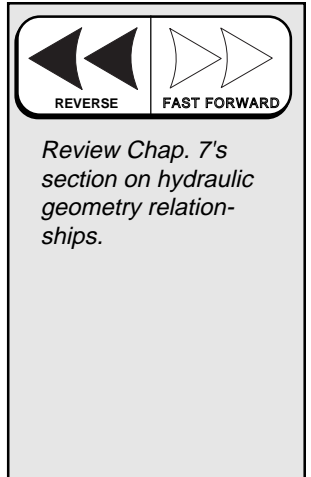
Table 8.2: Selected analytical procedures for stable channel design.

Stable Channel Method		Domain	Resistance Equation	Sediment Transport Equation	Third Relation
Copeland	1994	Sand-bed rivers	Brownlie	Brownlie	Left to designer's discretion
Chang	1988	Sand-bed rivers	Various	Various	Minimum stream power
Chang	1988	Gravel-bed rivers	Bray	Chang (similar in form to Parker, Einstein)	Minimum slope
Abou-Saida and Saleh	1987	Sand-bed canals	Liu-Hwang	Einstein-Brown	Left to designer's discretion
White et al.	1981	Sand-bed rivers	White et al.	Ackers-White	Maximum sediment transport
Griffiths	1981	Gravel-bed rivers	Griffiths	Shields entrainment	Empirical stability index

geometry formulas. To specify a value for the force "required to initiate motion," the designer must resort to empirical relationships between sediment size and critical shear stress. In fact, the only difference between the tractive stress approach for design stability analysis and the allowable stress approach is that the effect of cross-sectional shape (in particular, the bank angles) is considered in the former (**Figure 8.24**). Effects of turbulence and secondary currents are poorly represented in this approach.

Tractive stress approaches typically presume constant discharge, zero bed material sediment transport, and straight, prismatic channels and are therefore poorly suited for channels with moving beds. Additional limitations of the tractive stress design approach are discussed by Brookes (1988) and USACE (1994). Tractive stress approaches are appropriate for designing features made of rock or gravel (artificial riffles, revetments, etc.) that are expected to be immobile.

Figure 8.24: Low energy system with small bank angles.
Bank angles need to be considered when using the tractive stress approach.

Channels with Moving Beds and Known Slope

More general analytical approaches for designing channels with bed material discharge reduce the number of variables by assuming certain constant values (such as a trapezoidal cross-sectional shape or bed sediment size distribution) and by adding new equations based on an extremal hypothesis (Bettess and White 1987). For example, in a refinement of the tractive stress approach, Parker (1978) assumed that a stable gravel channel is characterized by threshold conditions only at the junction point between bed and banks. Using this assumption and including lateral diffusion of longitudinal momentum due to fluid turbulence in the analysis, he showed that points on the bank experience stresses less than threshold while the bed moves.

Following Parker's work, Ikeda et al. (1988) derived equations for stable width and depth (given slope and bed material gradation) of gravel channels with unvegetated banks composed of noncohesive material and flat beds in motion at bankfull. Channels were assumed to be nearly straight (sinuosity < 1.2) with trapezoidal cross sections free of alternate bars. In a subsequent paper Ikeda and Izumi (1990) extended the derivation to include effects of rigid bank vegetation.

Extremal hypotheses state that a stable channel will adopt dimensions that lead to minimization or maximization of some quantity subject to constraints imposed by the two governing equations (e.g., sediment transport and flow resistance). Chang (1988) combined sediment transport

and flow resistance formulas with flow continuity and minimization of stream power at each cross section and through a reach to generate a numerical model of flow and sediment transport. Special relationships for flow and transverse sediment transport in bends were also derived. The model was used to make repeated computations of channel geometry with various values for input variables. Results of the analysis were used to construct a family of design curves that yield d (bankfull depth) and w (bankfull width), given bankfull Q, S, and D_{50}. Separate sets of curves are provided for sand and gravel bed rivers. Regime-type formulas have been fit to the curves, as shown in **Table 8.3**. These relationships should be used with tractive stress analyses to develop converging data that increase the designer's confidence that the appropriate channel dimensions have been selected.

Subsequent work by Thorne et al. (1988) modified these formulas to account for effects of bank vegetation along gravel-bed rivers. The Thorne et al. (1988) formulas in **Table 8.3** are based on the data presented by Hey and Thorne (1986) in **Table 7.6**.

Channels with Moving Beds and Known Sediment Concentration

White et al. (1982) present an analytical approach based on the Ackers and White sediment transport function, a companion flow resistance relationship, and maximization of sediment transport for a specified sediment concentration. Tables (White et al. 1981) are available to assist users in implementing this procedure. The tables contain entries for sediment

sizes from 0.06 to 100 millimeters, discharges up to 35,000 cubic feet per second, and sediment concentrations from 10 to 4,000 parts per million. However, this procedure is not recommended for gravel bed channels (USACE 1994). Sediment concentration at bankfull flow is required as an input variable, which limits the usefulness of this procedure. Procedures for computing sediment discharge, Q_S, are outlined in Chapter 7. Copeland (1994) found that the White et al. (1982) method for channel design was not robust for cohesive bed materials, artificial grade controls, and disequilibrium sediment transport. The method was also found inappropriate for an unstable, high-energy ephemeral sand-bed stream (Copeland 1994). However, Hey (1990) found the Ackers-White sediment transport function performed well when analyzing stability of 18 flood control channels in Britain.

The approach described by Copeland (1994) features use of the Brownlie (1981) flow-resistance and sediment-transport relations, in the form of the software package "SAM" (Thomas et al. 1993). Additional features include the determination of input bed material concentration by computing sediment concentration from hydraulic parameters for an upstream "supply reach" represented by a bed slope, a trapezoidal cross section, bed-material gradation, and a discharge. Bank and bed roughness are composited using the equal velocity method (Chow 1959) to obtain roughness for a cross section. A family of slope-width solutions that satisfy the flow resistance and sediment transport relations are then computed. The designer then selects

Table 8.3: Equations for river width and depth.

Author	Year	Data	Domain	k_1	k_2	k_4
Chang	1988		Meandering or braided sand-bed rivers with:			
		Equiwidth point-bar streams and stable canals	$0.00238 < SD_{50}^{-0.5} Q^{-0.51}$ and $SD_{50}^{-0.5} Q^{-0.55} < 0.05$	$3.49k_1*$		$3.51k_4*$
		Straight braided streams	$0.05 < SD_{50}^{-0.5} Q^{-0.55}$ and $SD_{50}^{-0.5} Q^{-0.51} < 0.047$	Unknown and unusual		
		Braided point-bar and wide-bend point-bar streams; beyond upper limit lie steep, braided streams	$0.047 < SD_{50}^{-0.5} Q^{-0.51} <$ indefinite upper limit	$33.2k_1**$	0.93	$1.0k_4**$
Thorne et al.	1988	Same as for Thorne and Hey 1986	Gravel-bed rivers	$1.905 + k_1***$	0.47	$0.2077 + k_4***$
		Adjustments for bank vegetation[a]	Grassy banks with no trees or shrubs	$w = 1.46 w_c - 0.8317$		$d = 0.8815 d_c + 0.2106$
			1-5% tree and shrub cover	$w = 1.306 w_c - 8.7307$		$d = 0.5026 d_c + 1.7553$
			5-50% tree and shrub cover	$w = 1.161 w_c - 16.8307$		$d = 0.5413 d_c + 2.7159$
			Greater than 50% tree and shrub cover, or incised into flood plain	$w = 0.9656 w_c - 10.6102$		$d = 0.7648 d_c + 1.4554$

Chang equations for determining river width and depth. Coefficients for equations of the form $w = k_1 Q^{K_2}$; $d = K_4 Q^{K5}$; where w is mean bankfull width (ft), Q is the b
    or dominant discharge ($ft^3/_s$), d is mean bankfull depth (ft), D_{50} is median bed-material size (mm), and S is slope (ft/ft).

[a] w_c and d_c in these equations are calculated using exponents and coefficients from the row labeled "gravel-bed rivers".

$k_1* = (S D_{50}^{-0.5} - 0.00238Q^{-0.51})^{0.02}$.

$k_4* = \exp[-0.38 (420.17S D_{50}^{-0.5}Q^{-0.51} -1)^{0.4}]$.

$k_1** = (S D_{50}^{-0.5})^{0.84}$.

$k_4** = 0.015 - 0.025 \ln Q - 0.049 \ln (S D_{50}^{-0.5})$.

$k_1*** = 0.2490[\ln(0.0010647D_{50}^{1.15}/SQ^{0.42})]^2$.

$k_4*** = 0.2418 \ln(0.0004419D_{50}^{1.15}/SQ^{0.42})$.

any combination of channel properties that are represented by a point on the slope-width curve. Selection may be based on minimum stream power, maximum possible slope, width constraint due to right-of-way, or maximum allowable depth. The current (1996) version of the Copeland procedure assumes a straight channel with a trapezoidal cross section and omits the portion of the cross section above side slopes when computing sediment discharge. Effects of bank vegetation are considered in the assigned roughness coefficient.

The Copeland procedure was tested by application to two existing stream channels, the Big and Colewa Creeks in Louisiana and Rio Puerco in New Mexico (Copeland 1994). Considerable professional judgment was used in selection of input parameters. The Copeland method was found inapplicable to the Big and Colewa Creeks (relatively stable perennial streams with sand-clay beds), but applicable to Rio Puerco (high-energy, ephemeral sand-bed stream with stable profile and unstable banks). This result is not surprising since all stable channel design methods developed to date presume alluvial (not cohesive or bedrock) beds.

Use of Channel Models for Design Verification

In general, a model can be envisioned as a system by whose operation the characteristics of other similar systems may be predicted. This definition is general and applies to both hydraulic (physical) and computational (mathematical) models. The use and operation of computer models has improved in recent years as a result of better knowledge of fluvial hydraulics and the development of sophisticated digital control and data acquisition systems.

Any stream corridor restoration design needs careful scrutiny because its long-term impact on the stream system is not easy to predict. Sound engineering often dictates the use of computer models or physical models to check the validity of a proposed design. Since most practitioners do not have easy access to physical modeling facilities, computer models are much more widely used. Computer models can be run in a qualitative mode with very little data or in a highly precise quantitative mode with a great deal of field data for calibration and verification.

Computer models can be used to easily and cheaply test the stability of a restoration design for a range of conditions, or for a variety of alternative channel configurations. A "model" can vary in cost from several hundred dollars to several hundred thousand dollars, depending on what model is used, the data input, the degree of precision required, and the length and complexity of the reach to be modeled. The decision as to what models are appropriate should be made by a hydraulic engineer with a background in sediment transport.

The costs of modeling could be small compared to the cost of redesign or reconstruction due to failure. If the consequences of a project failure would result in a high risk of catastrophic damage or death, and the site-specific conditions result in an unacceptable level of uncertainty when

applying computer models, a physical model is the appropriate tool to use for design.

Physical Models

In some instances, restoration designs can become sufficiently complicated to exceed the capabilities of available computational models. In other situations, time might be of the essence, thus precluding the development of new computational modeling capabilities. In such cases the designer must resort to physical modeling for verification.

Depending on the scaling criteria used to achieve similitude, physical models can be classified as distorted, fixed, or movable-bed models. The theory and practice of physical modeling are covered in detail by French (1985), Jansen et al. (1979), and Yalin (1971) and are beyond the scope of this document. Physical modeling, like computational modeling, is a technology that requires specialized expertise and considerable experience. The U.S.

Army Waterways Experiment Station, Vicksburg, Mississippi, has extensively developed the technique of designing and applying physical models of rivers.

Computer Models

Computer models are structured and operated in the same way as a physical model (**Figure 8.25**). One part of the code defines the channel planform, the bathymetry, and the material properties of transported constituents. Other parts of the code create conditions at the boundaries, taking the place of the limiting walls and flow controls in the physical model. At the core of the computer code are the water and sediment transport solvers. "Turning on" these solvers is equivalent to running the physical model. At the end of the simulation run the new channel bathymetry and morphology are described by the model output. This section summarizes computational channel models that can be useful for evaluation of stream corridor restoration designs. Since it is not possible to include every existing model in the space available, the discussion here is limited to a few selected models (**Table 8.4**). In addition, Garcia et al. (1994) review mathematical models of meander bend migration.

These models are characterized as having general applicability to a particular class of problems and are generally available for desktop computers using DOS operating systems. Their conceptual and numerical schemes are robust, having been proven in field applications, and the code can be successfully used by

Figure 8.25: Use of models for design evaluation.
Modeling helps evaluate economics and effectiveness of alternative designs.
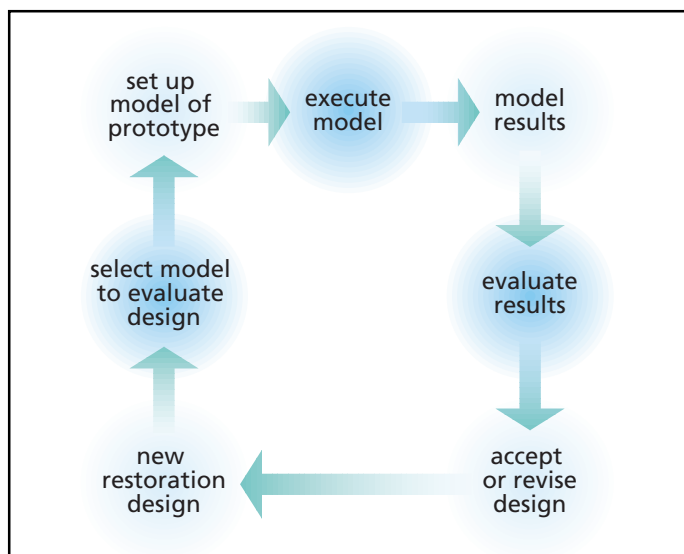
Table 8.4: Examples of computational models.

Model	CHARIMA	Fluvial-12	HEC-6	TABS-2	Meander	USGS	D•O•T	GSTARS
Discretization and formulation:								
Unsteady flow | stepped hydrograph	Y | Y	Y | Y	N | Y	Y | Y	N | Y	Y | Y	N | Y	N | Y
One-dimensional | quasi-two-dimensional	Y | N	Y | Y	Y | N	N | N	N | N	N	Y | Y	Y | Y
Two-dimensional, depth-average flow	N	N	N	Y	Y	Y | Y	N	N | Y
Deformable bed | banks	Y | N	Y | Y	Y | N	Y | N	Y | N	Y | N	Y | Y	Y | Y
Graded sediment load	Y	Y	Y	Y	Y	N	Y	Y
Nonuniform grid	Y	Y	Y	Y	Y	Y	Y	Y
Variable time stepping	Y	N	Y	N	N	N	N	Y
Numerical solution scheme:								
Standard step method	N	Y	Y	N	N	N	Y	Y
Finite difference	Y	N	Y	N	Y	Y	Y	Y
Finite element	N	N	N	Y	N	N	N	N
Modeling capabilities								
Upstream water and sediment hydrographs	Y	Y	Y	Y	Y	Y	Y	Y
Downstream stage specification	Y	Y	Y	Y	Y	N	Y	Y
Floodplain sedimentation	N	N	N	Y	N	N	N	N
Suspended | total sediment transport	Y | N	Y | N	N | Y	Y | N	N | N	N | Y	N | Y	N | Y
Bedload transport	Y	Y	Y	N	Y	N	N	Y
Cohesive sediments	N	N	Y	Y	N	Y	N	Y
Bed armoring	Y	Y	Y	N	N	N	Y	Y
Hydraulic sorting of substrate material	Y	Y	Y	N	N	N	Y	Y
Fluvial erosion of streambanks	N	Y	N	N	N	N	Y	Y
Bank mass failure under gravity	N	N	N	N	N	N	Y	N
Straight | irregular nonprismatic reaches	Y | N	Y | N	Y | N	Y | Y	N | N	N | N	Y | Y	Y | Y
Branched | looped channel network	Y | Y	Y | N	Y | N	Y | Y	N | N	N | N	N | N	N | N
Channel beds	N	Y	N	Y	Y	N	Y	N
Meandering belts	N	N	N	N	N	Y	N	N
Rivers	Y	Y	Y	Y	Y	Y	Y	Y
Bridge crossings	N	N	N	Y	N	N	N	N
Reservoirs	N	Y	Y	N	N	N	N	Y
User support								
Model documentation	Y	Y	Y	Y	Y	Y	Y	Y
User guide | hot-line support	N | N	Y | N	Y | Y	Y | N	N | N	Y | N	N | N	Y | N

Y = Yes
N = No

persons without detailed knowledge of the core computational techniques. Examples of these models and their features are summarized in **Table 8.4**. The acronyms in the column titles identify the following models: CHARIMA (Holly et al. 1990), FLUVIAL-12 (Chang 1990), HEC-6 (HEC 1991), TABS-2 (Williams and McAnally 1985), MEANDER (Johannesson and Parker 1985), USGS (Nelson and Smith 1989), D-O-T (Darby and Thorne 1996, Osman and Thorne 1988), GSTARS (Molinas and Yang 1996) and GSTARS 2.0 (Yang et al. 1998). GSTARS 2.0 is an enhanced and improved PC version of GSTARS. HEC-6, TABS-2, and USGS are federal, public domain models, whereas CHARIMA, FLUVIAL-12, MEANDER, and D-O-T are academic, privately owned models.

With the exception of MEANDER, all the above models calculate at each computational node the fractional sediment load and rate of bed aggradation or degradation, and update the channel topography. Some of them can simulate armoring of the bed surface and hydraulic sorting (mixing) of the underlying substrate material. CHARIMA, FLUVIAL-12, HEC-6, and D-O-T can simulate transport of sands and gravels. TABS-2 can be applied to cohesive sediments (clays and silts) and sand sediments that are well mixed over the water column. USGS is specially designed for gravel bed-load transport. FLUVIAL-12 and HEC-6 can be used for reservoir sedimentation studies. GSTARS 2.0 can simulate bank failure.

Comprehensive reviews on the capabilities and performance of these and other existing channel models are provided in reports by the National Research Council (1983), Fan (1988), Darby and Thorne (1992), and Fan and Yen (1993).

Detailed Design

Channel Shape

Natural stream width varies continuously in the longitudinal direction, and depth, bed slope, and bed material size vary continuously along the horizontal plane. These variations give rise to natural heterogeneity and patterns of velocity and bed sediment size distribution that are important to aquatic ecosystems.

Widths, depths, and slopes computed during design should be adopted as reach mean values, and restored channels should be constructed with asymmetric cross sections (Hunt and Graham 1975, Keller 1978, Iversen et al. 1993, MacBroom 1981) (**Figure 8.26**). Similarly, meander planform should vary from bend to bend about average values of arc length and radius. A reconstructed floodplain should not be perfectly flat (**Figure 8.27**).

Channel Longitudinal Profile and Riffle Spacing

In stream channels with significant amounts of gravel ($D_{50} > 3$ mm) (Higginson and Johnston 1989), riffles should be associated with steep zones near meander inflection points. Riffles are not found in channels with beds of finer materials. Studies conducted by Keller and Melhorn (1978) and confirmed by Hey and Thorne (1986) indicate *pool-riffle spacing* should

vary between 3 and 10 channel widths and average about 6 channel widths even in bedrock channels. More recent work by Roy and Abrahams (1980) and Higginson and Johnston (1989) indicates that pool-riffle spacing varies widely within a given channel.

Average riffle spacing is often (but not always) half the meander length since riffles tend to occur at meander inflection points or crossovers. Riffles sometimes appear in groups or clusters. Hey and Thorne (1986) analyzed data from 62 sites on gravel-bed rivers in the United Kingdom and found riffle spacing varied from 4 to 10 channel widths with the least squares best fit at 6.31 channel widths. Riffle spacing tends to be nearer 4 channel widths on steeper gradients and 8 to 9 channel widths on more gradual slopes (R.D. Hey, personal communication). Hey and Thorne (1986) also developed regression formulas for riffle width, mean depth, and maximum depth.

Stability Assessment

The risk of a restored channel being damaged or destroyed by erosion or deposition is an important consideration for almost all restoration work. Designers of restored streams are confronted with rather high levels of uncertainty. In some cases, it may be wise for designers to compute risk of failure by calculating the joint probability of design assumptions being false, design equation inaccuracy, and occurrence of extreme hydrologic events during project life. Good design practice also requires checking channel performance at discharges well above and below the design
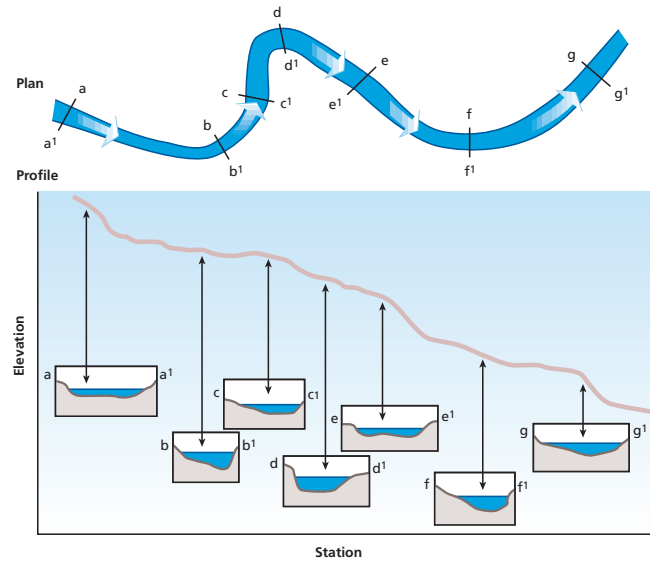

Figure 8.26: Example plan and profile of a naturally meandering stream.
Channel cross sections vary based on width, depth, and slope.

condition. A number of approaches are available for checking both the vertical (bed) and horizontal (bank) stability of a designed stream. These stability checks are an important part of the design process.

Vertical (Bed) Stability

Bed stability is generally a prerequisite for bank stability. Aggrading channels are liable to braid or exhibit accelerated lateral migration in response to middle or point bar growth. Degrading channels widen explosively when bank heights and angles exceed a critical threshold specific to bank soil

Figure 8.27: A stream meander and raised floodplain.
Natural floodplains rise slightly between a crossover and an apex of a meander.

type. Bed aggradation can be addressed by stabilizing eroding channels upstream, controlling erosion on the watershed, or installing sediment traps, ponds (Haan et al. 1994), or debris basins (USACE 1989b). If aggradation is primarily due to deposition of fines, it can be addressed by narrowing the channel, although a narrower channel might require more bank stabilization.

If bed degradation is occurring or expected to occur, and if modification is planned, the restoration initiative should include flow modification, grade control measures, or other approaches that reduce the energy gradient or the energy of flow. There are many types of grade control structures. The applicability of a particular type of structure to a specific restoration depends on a number of factors, such as hydrologic conditions, sediment size and loading, channel morphology, floodplain and valley characteristics, availability of construction materials, ecological objectives, and time and funding constraints. For more information on various structure designs, refer to Neilson et. al. (1991), which provides a comprehensive literature review on grade control structures with an annotated bibliography. Grouted boulders can be used as a grade control structure. They are a key component in the successful restoration of the South Platte River corridor in Denver, Colorado (McLaughlin Water Engineers, Ltd., 1986).

Grade control structure stilling basins can be valuable habitats in severely degraded warm water streams (Cooper and Knight 1987, Shields and Hoover 1991). Newbury and Gaboury (1993) describe the construction of artificial riffles that serve as bed degradation controls. Kern (1992) used "river bottom ramps" to control bed degradation in a River Danube meander restoration initiative. Ferguson (1991) reviews creative designs for grade control structures that improve streamside habitat and aesthetic resources (**Figure 8.28**).

Figure 8.28: Grade control structure.

Control measures can double as habitat restoration devices and aesthetic features.

Horizontal (Bank) Stability

Bank stabilization may be necessary in restored channels due to floodplain land uses or because constructed banks are more prone to erosion than "seasoned" ones, but it is less than ideal if ecosystem restoration is the objective. Floodplain plant communities owe their diversity to physical processes that include erosion and deposition associated with lateral migration (Henderson 1986). Bank erosion control methods must be selected with the dominant erosion mechanisms in mind (Shields and Aziz 1992).

Bank stabilization can generally be grouped into one of the following

three categories: (1) indirect methods, (2) surface armor, and (3) vegetative methods. Armor is a protective material in direct contact with the streambank. Armor can be categorized as stone, other self-adjusting armor (sacks, blocks, rubble, etc.), rigid armor (concrete, soil cement, grouted riprap, etc.) and flexible mattress (gabions, concrete blocks, etc.). Indirect methods extend into the stream channel and redirect the flow so that hydraulic forces at the channel boundary are reduced to a nonerosive level. Indirect methods can be classified as dikes (permeable and impermeable) and other flow deflectors such as bendway weirs, stream "barbs," and Iowa vanes. Vegetative methods can function as either armor or indirect protection and in some applications can function as both simultaneously. A fourth category is composed of techniques to correct problems caused by geotechnical instabilities.

Guidance on selection and design of bank protection measures is provided by Hemphill and Bramley (1989) and Henderson (1986). Coppin and Richards (1990), USDA-NRCS (1995), and Shields et al. (1995d) provide additional detail on the use of vegetative techniques (see following section). Newly constructed channels are more susceptible to bank erosion than older existing channels, with similar inflows and geometries, due to the influence of vegetation, armoring, and the seasoning effect of clay deposition on banks (Chow 1959). In most cases, outer banks of restored or newly constructed meanders will require protection. Structural techniques are needed (e.g., Thorne et al. 1995) if immediate stability is re-

quired, but these may incorporate living components. If time permits, the new channel may be constructed "in the dry" and banks planted with woody vegetation. After allowing the vegetation several growing seasons to develop, the stream may be diverted in from the existing channel (R.D. Hey, personal communication).

Bank Stability Check

Outer banks of meanders erode, but erosion rates vary greatly from stream to stream and bend to bend. Observation of the project stream and similar reaches, combined with professional judgment, may be used to determine the need for bank protection, or erosion may be estimated by simple rules of thumb based largely on studies that relate bend migration rates to bend geometry (e.g., Apmann 1972 and review by Odgaard 1987) (**Figure 8.29**). More accurate prediction of the rate of erosion of a given streambank is at or beyond the current state of the art. No standard methods exist, but several recently developed tools are

Figure 8.29: Channel exhibiting accelerated lateral migration.
Erosion of an outer bank on the Missouri River is a natural process; however the rate of erosion should be monitored.

available. None of these have been used in extremely diverse settings, and users should view them with caution.

Tools for predicting bank erosion may be divided into two groups: (1) those which predict erosion primarily due to the action of water on the streambank surface and (2) those which focus on subsurface geotechnical characteristics.

Figure 8.30: Bank failure stages.

Stability of a bank will vary from stable to unstable depending on bank height, bank angle, and soil conditions.


Among the former is an index of streambank erodibility based on field observations of emergency spillways (Temple and Moore 1995). Erosion is predicted for sites where a power number based on velocity, depth, and bend geometry exceeds an erodibility index computed from tabulated values of streambank material properties. Also among this group are analytical models such as the one developed by Odgaard (1989), which contain rather sophisticated representations of flow fields, but require input of an empirical constant to quantify soil and vegetation properties. These models should be applied with careful consideration of their limitations. For example, Odgaard's model should not be applied to bends with "large curvature."

The second group of predictive tools focuses on banks that undergo mass failure due to geotechnical processes. Side slopes of deep channels may be high and steep enough to be geotechnically unstable and to fail under the influence of gravity. Fluvial processes in such a situation serve primarily to remove blocks of failed material from the bank toe, leading to a resteepened bank profile and a new cycle of failure, as shown in **Figure 8.30**. Study of bank failure processes along incised channels has led to a procedure for relating bank geometry to stability for a given set of soil conditions (Osman and Thorne 1988, Thorne and Osman 1988). If banks of a proposed design channel are to be higher than about 10 feet, stability analysis should be conducted. These analyses are described in detail in Chapter 7. Bank height estimates should allow for scour along the
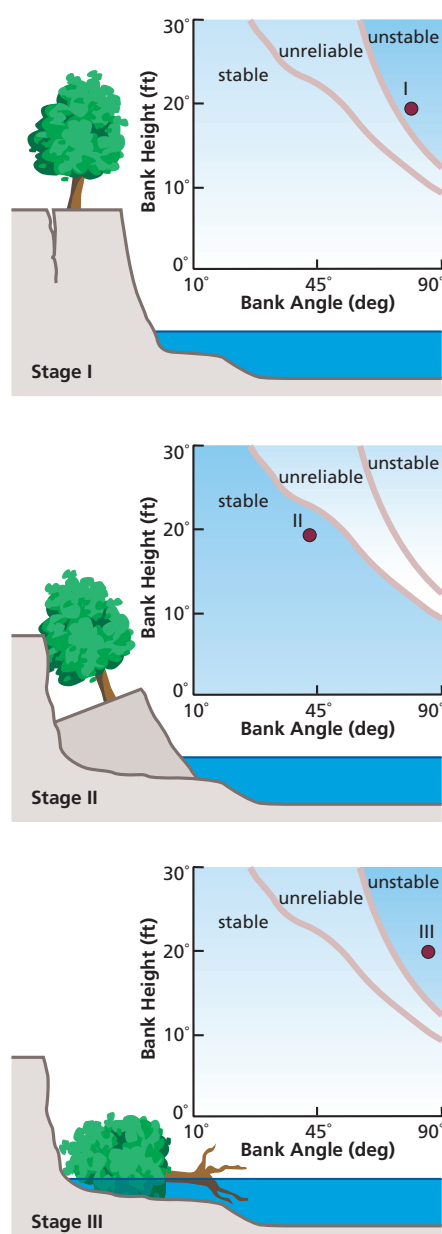
outside of bends. High, steep banks are also susceptible to internal erosion, or piping, as well as streambanks of soils with high dispersion rates.

Allowable Velocity Check

Fortier and Scobey (1926) published tables regarding the maximum nonscouring velocity for given channel boundary materials. Different versions of these tables have appeared in numerous subsequent documents, notably Simons and Senturk (1977) and USACE (1991). The applicability of these tables is limited to relatively straight silt and sand-bed channels with depths of flow less than 3 feet and very low bed material loads. Adjustments to velocities have been suggested for situations departing from those specified. Although slight refinements have been made, these data still form the basis of the allowable velocity approach.

Figure 8.31 contains a series of graphs that summarize the tables and aid in selecting correction factors for flow depth, sediment concentration, flow frequency, channel curvature, bank slope, and channel boundary soil properties. Use of the allowable velocity approach is not recommended for channels transporting a significant load of material larger than 1 mm. The restoration design, however should also consider the effects of hydraulic roughness and the protection afforded by vegetation.

Perhaps because of its simplicity, the allowable velocity method has been used directly or in slightly modified form for many restoration applications. Miller et al. (1983) used allowable velocity criteria to design man-made gravel riffles located immediately downstream of a dam releasing a constant discharge of sediment-free water. Shields (1983) suggested using allowable velocity criteria to size individual boulders placed in channels to serve as instream habitat structures. Tarquin and Baeder (1983) present a design approach based on allowable velocity for low-order ephemeral streams in Wyoming landscapes disturbed by surface mining. Velocity of the design event (10-year recurrence interval) was manipulated by adjusting channel length (and thus slope), width, and roughness. Channel roughness was adjusted by adding meanders, planting shrubs, and adding coarse bed material. The channel width-to-depth ratio design was based on the pre-mining channel configuration.

Allowable Stress Check

Since boundary shear stress is more appropriate than velocity as a measure of the forces driving erosion, graphs have also been developed for allowable shear stress. The average boundary shear stress acting on an open channel conveying a uniform flow of water is given by the product of the unit weight of water (γ, lb/ft^3) times the hydraulic radius (R, ft) times the bed slope S:

$$\tau = \gamma RS$$

Figure 8.32 is an example of allowable shear stress criteria presented in graphical form. The most famous graphical presentation of allowable shear stress criteria is the Shields diagram, which depicts conditions necessary for initial movement of noncohesive particles on a flat bed straight channel in terms of dimension-

Figure 8.31: Allowable velocities for unprotected earth channels.

Curves reflect practical experience in design of stable earth channels.

Source: USDA Soil Conservation Service 1977.

Correction Factor F — frequency of design flow
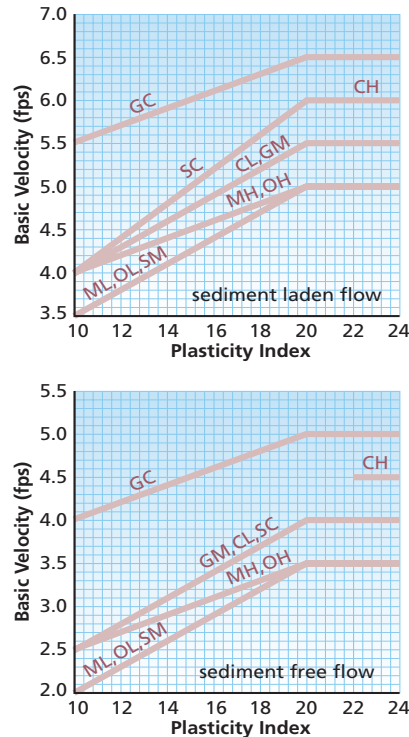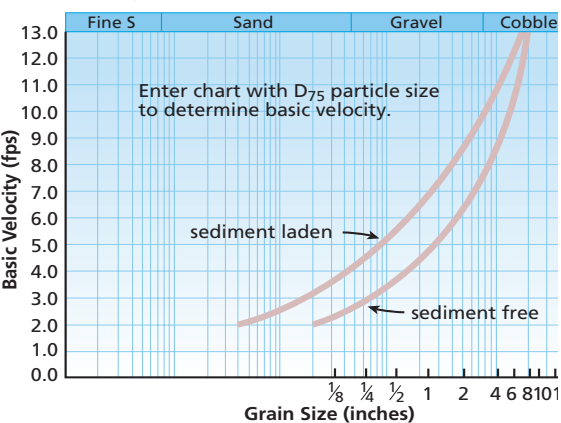
Flood Frequency (percent chance)

Correction Factor A — alignment

Curve Radius ÷ Water Surface Width

Correction Factor D — depth of design flow

Water Depth (feet)

Correction Factor B — bank slope

Cotangent of Slope Angle (z)

Notes:
In no case should the allowable velocity be exceeded when the 1% chance discharge occu regardless of the desi flow frequency.

Correction Factor C_e — density

SM,SC,GM,GC   CH,MH   CL,ML

Void Ratio (e)

Basic Velocities for Coherent Earth Materials (v_b)

Basic Velocity (fps)

GC   CH   SC   CL,GM   MH,OH   ML,OL,SM

sediment laden flow

Plasticity Index

Basic Velocity for Discrete Particles of Earth Materials

Fine S | Sand | Gravel | Cobble

Enter chart with D_{75} particle size to determine basic velocity.

sediment laden

sediment free

Grain Size (inches)

Basic Velocity (fps)

GC   CH   GM,CL,SC   MH,OH   ML,OL,SM

sediment free flow

Plasticity Index

| Allowable Velocities for Unprotected Earth Channels	
Channel Boundary Materials	**Allowable Velocity**
Discrete Particles	
Sediment Laden Flow	
$D_{75} > 0.4$mm	basic velocity chart value x D x A x
$D_{75} < 0.4$mm	2.0 fps
Sediment Free Flow	
$D_{75} > 0.2$mm	basic velocity chart value x D x A x
$D_{75} < 0.2$mm	2.0 fps
Coherent Earth Materials	
PI > 10	basic velocity chart value x D x A x F
PI < 10	2.0 fps

less variables (Vanoni 1975). The Shields curve and other allowable shear stress criteria (e.g., Figure10.5, Henderson 1966; Figure 7.7, Simons and Senturk 1977) are based on laboratory and field data. In simplest form, the Shields criterion for channel stability is (Henderson 1966):

$$RS/[(S_S-1)D_S] < \text{a constant}$$

$$\text{for } D_S > \sim 6 \text{ mm}$$

where S_s is the specific gravity of the sediment and D_S is a characteristic bed sediment size, usually taken as the median size, D_{50}, for widely graded material. Note that the hydraulic radius, R, and the characteristic bed sediment size, D_S, must be in the same units for the Shields constant to be dimensionless. The dimensionless constant is based on measurements and varies from 0.03 to 0.06 depending on the data set used to determine it and the judgment of the user (USACE 1994).

These constant values are for straight channels with flat beds (no dunes or other bedforms). In natural streams, bedforms are usually present, and values of this dimensionless constant required to cause entrainment of bed material may be greater than 0.06. It should be noted that entrainment does not imply channel erosion. Erosion will occur only if the supply of sediment from upstream is less than that transported away from the bed by the flow. However, based on a study of 24 gravel-bed rivers in the Rocky Mountain region of Colorado, Andrews (1984) concluded that stable gravel-bed channels cannot be maintained at values of the Shields constant greater than about 0.080. Smaller Shields constant values are more conservative
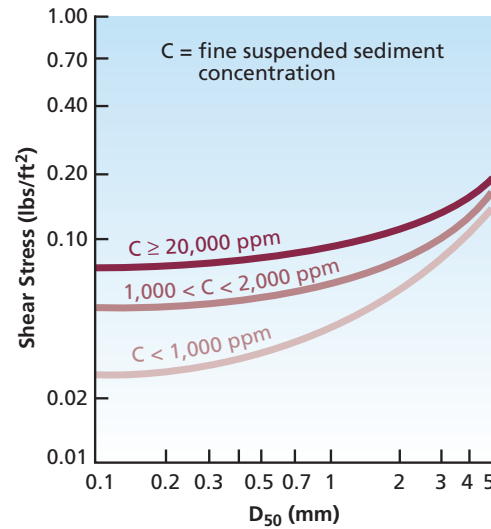
with regard to channel scour, but less conservative with regard to deposition. If $S_S = 2.65$, and the constant is assumed to be 0.06, the equation above simplifies to $D_{50} = 10.1RS$.

Allowable shear stress criteria are not very useful for design of channels with beds dominated by sand or finer materials. Sand beds are generally in motion at design discharge and have dunes, and their shear stress values are much larger than those indicated by the Shields criterion, which is for incipient motion on a plane bed. Allowable shear stress data for cohesive materials show more scatter than those for sands and gravels (Grissinger et al. 1981, Raudkivi and Tan 1984), and experience and observation with local channels are preferred to published charts like those shown in Chow (1959). Models of cohesive soil erosion require field or laboratory evaluation of model parameters or constants. Extrapolation of laboratory flume results to field conditions is difficult, and even field tests are subject to site-specific influences. Erosivity of cohesive soils is affected

Figure 8.32: Allowable mean shear stress for channels with boundaries of noncohesive material larger than 5 mm carrying negligible bed material load.
Shear stress diminishes with increased suspended sediment concentrations.
From Lane 1955.

by the chemical composition of the soil, the soil water, and the stream, among other factors.

However, regional shear stress criteria may be developed from observations of channels with sand and clay beds. For example, USACE (1993) determined that reaches in the Coldwater River Watershed in northwest Mississippi should be stable with an average boundary shear stress at channel-forming (2-year) discharge of 0.4 to 0.9 lb/ft^2.

The value of the Shields constant also varies with bed material size distribution, particularly for paved or armored beds. Andrews (1983) derived a regression relationship that can be expressed as:

$$RS/[(S_S-1)D_i] < 0.0834 (D_i/D_{50})^{-0.0872}$$

When the left side of the above expression equals the right, bed-sediment particles of size D_i are at the threshold of motion. The D_{50} value in the above expression is the median size of subsurface material. Therefore, if $D_{50} = 30$ mm, particles with a diameter of 100 mm will be entrained when the left side of the above equation exceeds 0.029. This equation is for self-formed rivers that have naturally sorted gravel and cobble bed material. The equation holds for values of D_i/D_{50} between 0.3 and 4.2. It should be noted that R and D_i on the left side of the above equation must be expressed in the same units.

Practical Guidance: Allowable Velocity and Shear Stress

Practical guidance for application of allowable velocity and shear stress

approaches is provided by the Natural Resources Conservation Service (NRCS), formerly the U.S. Soil Conservation Service (SCS)(1977), and USACE (1994). See **Figure 8.31**.

Since form roughness due to sand dunes, vegetation, woody debris, and large geologic features in streams dissipates energy, allowable shear stress for bed stability may be higher than indicated by laboratory flume data or data from uniform channels. It is important to compute cross-sectional average velocities or shear stresses over a range of discharges and for seasonal changes in the erosion resistance of bank materials, rather than for a single design condition. Frequency and duration of discharges causing erosion are important factors in stability determination. In cobble- or boulder-bed streams, bed movement sometimes occurs only for discharges with return periods of several years.

Computing velocity or shear stress from discharge requires design cross sections, slope, and flow resistance data. If the design channel is not extremely uniform, typical or average conditions for rather short channel reaches should be considered. In channels with bends, variations in shear stress across the section can lead to scour and deposition even when average shear stress values are within allowable limits. The NRCS (formerly SCS) (1977) gives adjustment factors for channel curvature in graphical form that are based on very limited data (see **Figure 8.31**). Velocity distributions and stage-discharge relations for compound channels are complex (Williams and Julien 1989, Myers and Lyness 1994).

Allowable velocity or shear stress criteria should be applied to in-channel flow for a compound cross section with overbank flow, not cross-sectional average conditions (USACE 1994). Channel flow resistance predictors that allow for changing conditions with changing discharge and stage (e.g., Brownlie 1983 for sand-bed channels) should be used rather than constant resistance values.

If the existing channel is stable, design channel slope, cross section, and roughness may be adjusted so that the current and proposed systems have matching curves of velocity versus discharge (USACE 1994). This approach, while based on allowable velocity concepts, releases the procedure from published empirical values collected in other rivers that might be intrinsically different from the one in question.

Allowable Stream Power or Slope

Brookes (1990) suggested the product of bankfull velocity and shear stress, which is equal to the stream power per unit bed area, as a criterion for stability in stream restoration initiatives. This is based on experience with several restoration initiatives in Denmark and the United Kingdom with sandy banks, beds of glacial outwash sands, and a rather limited range of bankfull discharges (~15 to 70 cfs). These data are plotted as squares, triangles, and circles in **Figure 8.33**.

Brookes suggested that a stream power value of 2.4 ftlb/sec/ft^2 discriminated well between stable and unstable channels. Projects with stream powers less than about 1.0 ftlb/sec/ft^2 failed through deposition, whereas those

with stream powers greater than about 3.4 ftlb/sec/ft^2 failed through erosion.

Since these criteria are based on observation of a limited number of sites, application to different stream types (e.g., cobble-bed rivers) should be avoided. However, similar criteria may be developed for basins of interest. For example, data points representing stable reaches in the Coldwater River watershed of northwestern Mississippi are shown in Figure 8.34 as stars. This watershed is characterized by incised, straight (channelized) sand-bed channels with cohesive banks. Slopes for stable reaches were measured in the field, and 2-year discharges were computed using a watershed model (HEC-1) (USACE 1993).

Figure 8.33: Brookes' stream power stability criteria.
Stream power is the product of bankfull velocity and shear stress.
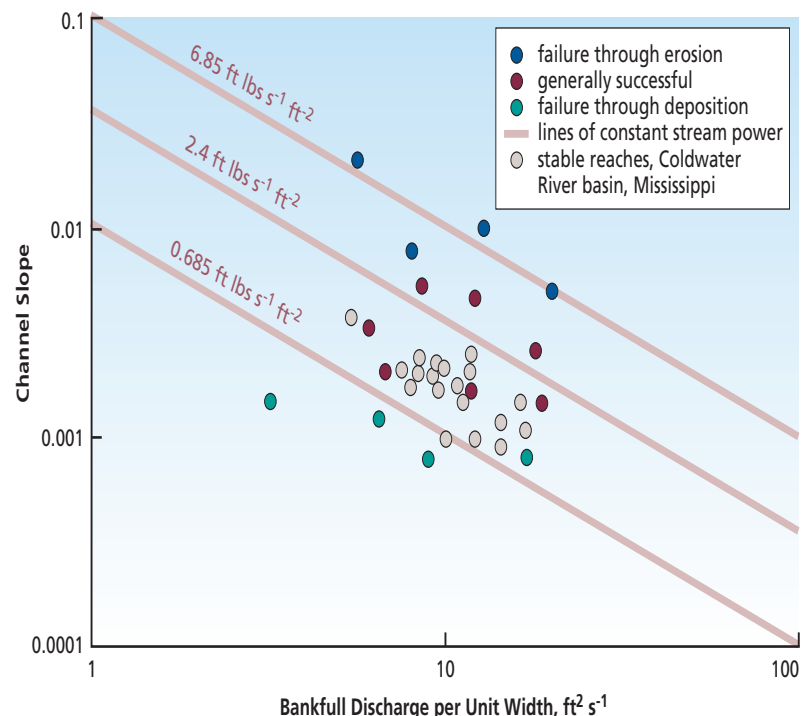
Allowable Shear Stress

The shape of the bed material size distribution is an important parameter for determining the threshold of motion of individual sediment sizes in a bed containing a mixture of sand and gravel. Beds composed of unimodal (particle-size distribution shows no secondary maxima) mixtures of sand and gravel were found to have a narrow range of threshold shear stresses for all sizes present on the bed surface. For unimodal beds, the threshold of motion of all grain sizes on the bed was found to be estimated adequately by using the Shields curve for the median grain size. Bed sediments composed of bimodal (particle-size distribution shows one secondary maximum) mixtures of sands and gravels were found to have threshold shear stresses that are still a function of grain size, although much less so than predicted by the Shields curve. For bed material with bimodal size distributions, using the Shields curve on individual grain sizes greater than the median size overestimates the threshold of motion and underestimates the threshold of motion for grain sizes less than the median size. Critical shear stresses for gravel beds may be elevated if gravels are tightly interlocked or imbedded.

Jackson and Van Haveren (1984) present an iterative technique for designing a restored channel based on allowable shear stress. Separate calculations were performed for channel bed and banks. Channel design included provision for gradual channel narrowing as the bank vegetation develops, and bank cohesion and resistance to erosion increase. Newbury and Gaboury (1993) use an allowable tractive force graph from Lane (1955) to check stability of channel restoration initiatives in Manitoba streams with cobble and gravel beds. Brookes (1991) gives an example of the application of this method for designing urban channels near London. From a practical standpoint, boundary shear stresses can be more difficult to measure and conceptualize than velocities (Brookes 1995). Allowable shear stress criteria may be converted to allowable velocities by including mean depth as a parameter.

The computed shear stress values are averages for the reach in question. Average values are exceeded at points, for example, on the outside of a bend.

Brookes' stream power criterion is one of several region-specific stability tests. Others include criteria based on slope and shear stress. Using empirical data and observation, the Corps of Engineers has developed relationships between slope and drainage area for various watersheds in northwestern Mississippi (USACE 1989c). For example, stable reaches in three watersheds had slopes that clustered around the regression line:

$$S = 0.0041 \, A^{-0.365}$$

where A is the contributing drainage area in square miles. Reaches with much steeper slopes tended to be degradational, while those with more gradual slopes tended to be aggradational. Downs (1995) developed stability criteria for channel reaches in the Thames Basin of the United Kingdom based entirely on slope: channels straightened during the 20th century were depositional if slopes were less than 0.005 and erosional if slopes were greater.

Sediment Yield and Delivery

Sediment Transport

If a channel is designed using an empirical or a tractive stress approach, computation of sediment-transport capacity allows a rough check to determine whether deposition is likely to be a problem. Sediment transport relationships are heavily dependent on the data used in their development. Inaccuracy may be reduced by selecting transport functions appropriate to the stream type and bed sediment size in question. Additional confidence can be achieved by obtaining calibration data; however, calibration data are not available from a channel yet to be constructed. If the existing channel is reasonably stable, designers can compute a sediment discharge versus streamflow relationship for the existing and proposed design channels using the same sediment transport function and try to match the curves as closely as possible (USACE 1994).

If information is available regarding sediment inflows into the new channel, a multiyear sediment budget can be computed to project likely erosion and deposition and possible maintenance needs. Sediment load can also be computed, using the hydraulic properties and bed material gradations of the upstream supply reach and a suitable sediment transport function. The USACE software SAM (Copeland 1994) includes routines that compute hydraulic properties for uniform flow and sediment discharge for single cross sections of straight channels using any of 13 different sediment transport functions. Cross sections may have complex geometry and boundary materials that vary along the section. Output can be combined with a hydrograph or a flow duration curve to obtain sediment load.

HEC-6 (USACE 1993) is a one-dimensional movable-boundary, open-channel-flow numerical model designed to simulate and predict changes in river profiles resulting from scour and deposition over moderate time periods, typically years, although applications to single flood events are possible. A continuous discharge record is partitioned into a series of steady flows of variable discharge and duration. For each discharge, a water surface profile is calculated, providing energy slope, velocity, depth, and other variables at each cross section. Potential sediment transport rates are then computed at each section. These rates, combined with the duration of the flow, permit a volumetric accounting of sediment within each reach. The amount of scour or deposition at each

section is then computed, and the cross section geometry is adjusted for the changing sediment volume. Computations then proceed to the next flow in the sequence, and the cycle is repeated using the updated cross section geometry. Sediment calculations are performed by grain size fractions, allowing the simulation of hydraulic sorting and armoring.

HEC-6 allows the designer to estimate long-term response of the channel to a predicted series of water and sediment supply. The primary limitation is that HEC-6 is one-dimensional, i.e., geometry is adjusted only in the vertical direction. Changes in channel width or planform cannot be simulated. Another Federal sediment routing model is the GSTARS 2.0 (Yang et al. 1998). GSTARS 2.0 can be used for a combination of subcritical and supercritical flow computations without interruption in a semi-two-dimensional manner. The use of stream tube concept in sediment routing enables GSTARS 2.0 to simulate channel geometry changes in a semi-three-dimensional manner.

The amount and type of sediment supplied to a stream channel is an important consideration in restoration because sediment is part of the balance (i.e., between energy and material load) that determines channel stability. A general lack of sediment relative to the amount of stream power, shear stress, or energy in the flow (indexes of transport capacity) usually results in erosion of sediment from the channel boundary of an alluvial channel. Conversely, an oversupply of sediment relative to the transport capacity of the flow usually results in deposition of sediment in that reach of stream.

Bed material sediment transport analyses are necessary whenever a restoration initiative involves reconstructing a length of stream exceeding two meander wavelengths. A reconstruction that modifies the size of a cross section and the sinuosity for such a length of channel should be analyzed to ensure that upstream sediment loads can be transported through the reconstructed reach with minimal deposition or erosion. Different storm events and the average annual transported bed material load also should be examined.

Sediment Discharge Functions

The selection of an appropriate discharge formula is an important consideration when attempting to predict sediment discharge in streams. Numerous sediment discharge formulas have been proposed, and extensive summaries are provided by Alonso (1980), Brownlie (1981), Yang (1996), Bathurst (1985), Gomez and Church (1989), Parker (1990), and Garbrecht et al. (1995).

Sediment discharge rates depend on flow velocity; energy slope; water temperature; size, gradation, specific gravity, and shape of the bed material and suspended-sediment particles; channel geometry and pattern; extent of bed surface covered by coarse material; rate of supply of fine material; and bed configuration. Large-scale variables such as hydrologic, geologic, and climatic conditions also affect the rate of sediment transport. Because of the range and number of variables, it is not possible to select a sediment transport formula that satisfactorily encompasses all the conditions that might be encountered. A specific formula might be more accurate than others when applied to a particular river, but it might not be accurate for other rivers.

Selection of a sediment transport formula should include the following considerations (modified from Yang 1996):

- Type of field data available or measurable within time, budget, and work hour limitations.
- Independent variables that can be determined from available data.
- Limitations of formulas versus field conditions.

If more than one formula can be used, the rate of sediment discharge should be calculated using each formula. The formulas that best agree with available measured sediment discharges should be used to estimate the rate of sediment discharge during flow conditions when actual measurements are not available.

The following formulas may be considered in the absence of any measured sediment discharges for comparison:

- Meyer-Peter and Muller (1948) formula when the bed material is coarser than 5 mm.
- Einstein (1950) formula when bed load is a substantial part of the total sediment discharge.
- Toffaleti (1968) formula for large sand-bed rivers.
- Colby (1964) formula for rivers with depths less than 10 feet and median bed material values less than 0.8 mm.

- Yang (1973) formula for fine to coarse sand-bed rivers.

- Yang (1984) formula for gravel transport when most of the bed material ranges from 2 to 10 mm.

- Ackers and White (1973) or Engelund and Hansen (1967) formula for sand-bed streams having subcritical flow.

- Laursen (1958) formula for shallow rivers with fine sand or coarse silt.

Available sediment data from a gaging station may be used to develop an empirical sediment discharge curve in the absence of a satisfactory sediment discharge formula, or to verify the sediment discharge trend from a selected formula. Measured sediment discharge or concentration should be plotted against streamflow, velocity, slope, depth, shear stress, stream power, or unit stream power. The curve with the least scatter and systematic deviation should be selected as the sediment rating curve for the station.

Sediment Budgets

A sediment budget is an accounting of sediment production in a watershed. It attempts to quantify processes of erosion, deposition, and transport in the basin. The quantities of erosion from all sources in a watershed are estimated using various procedures. Typically, the tons of erosion from the various sources are multiplied by sediment delivery ratios to estimate how much of the eroded soil actually enters a stream. The sediment delivered to the streams is then routed

through the watershed.

The sediment routing procedure involves estimating how much of the sediment in the stream ends up being deposited in lakes, reservoirs, wetlands, or floodplains or in the stream itself. An analysis of the soil textures by erosion process is used to convert the tons of sediment delivered to the stream into tons of silt and clay, sand, and gravel. Sediment transport processes are applied to help make decisions during the sediment routing analysis. The end result is the sediment yield at the mouth of the watershed or the beginning of a project reach.

Table 8.5 is a summary sediment budget for a watershed. Note that the information in the table may be from measured values, from estimates based on data from similar watersheds, or from model outputs (AGNPS, SWRRBWQ, SWAT, WEPP, RUSLE, and others. Contact the NRCS National Water and Climate Data Center for more information on these models). Sediment delivery ratios are determined for watershed drainage areas, based on sediment gauge data and reservoir sedimentation surveys.

The watershed is subdivided into subwatersheds at points where significant sediment deposition occurs, such as at bridge or road fills; where stream crossings cause channel and floodplain constrictions; and at reservoirs, lakes, significant flooded areas, etc. Sediment budgets similar to the table are constructed for each subwatershed so the sediment yield to the point of deposition can be quantified.

A sediment budget has many uses, including identification of sediment

Table 8.5: Example of a sediment budget for a watershed.

Protection Level	Erosion Source	Acres or Miles	Average Erosion Rate (tons/acre/year or tons/bank mile/year)	Annual Erosion (tons/ year)	Sediment Delivery Ratio (percent)	Sediment to Streams	Sediment Deposited Uplands & Floodplains (tons/year)	Sediment Delivered to Blue Stem Lake	
								(tons/ year)	(percent)
	Sheet, rill, and ephemeral gully								
Adequate	Cropland	6000	3.0	18,000	30	5400	14,380	3620	33.7
Inadequate	Cropland	1500	6.5	9750	30	2930	7790	1960	18.3
Adequate	Pasture/hayland	3400	1.0	3400	20	680	2940	460	4.3
Inadequate	Pasture/hayland	600	6.0	3600	20	720	3120	480	4.5
Adequate	Forestland	1200	0.5	600	20	120	520	80	0.7
Inadequate	Forestland	300	5.5	1650	20	330	1430	220	2.1
Adequate	Parkland	700	1.0	700	30	210	560	140	1.3
Inadequate	Parkland	0	0	0	30	0	0	0	0.0
Adequate	Other	420	2.0	840	20	170	730	110	1.0
Inadequate	Other	0	0	0	20	0	0	0	0.0
	Classic gully	N/A	N/A	600	40	240	440	160	1.5
	Streambank								
	Slight	14	50	100	700	5400	140	560	5.2
	Moderate	10.5	150	1580	100	1580	320	1260	11.7
	Severe	3.5	600	2100	100	2100	420	1680	15.7
			Total erosion	**43,520**			**Total sediment to Blue Stem Lake**	**10,730**	

Figure 8.34: Eroded upland area.

Upland sediment sources should be identified in a sediment budget.

sources for treatment (**Figure 8.34**). If the goal for a restoration initiative is to reduce sedimentation from a watershed, it is critical to know what type of erosion is producing the most sediment and where that erosion is occurring. In stream corridor restoration, sediment yield (both in terms of quantity and average grain size diameter) to a stream and its floodplain need to be identified and considered in designs. In channel stability investigations, the amount of sand and gravel sediment entering the stream from the watershed needs to be quantified to refine bed material transport calculations.

Example of a Sediment Budget

A simple application of a sediment transport equation in a field situation illustrates the use of a sediment budget. **Figure 8.35** shows a stream reach being evaluated for stability prior to developing a stream corridor restoration plan. Five representative channel cross sections (A, B, C, D, and E) are surveyed. Locations of the cross sections are selected to represent the reach above and below the points where tributary streams, D and E, enter the reach. Additional cross sections would need to be surveyed if the stream at A, B, C, D or E is not typical of the reach.

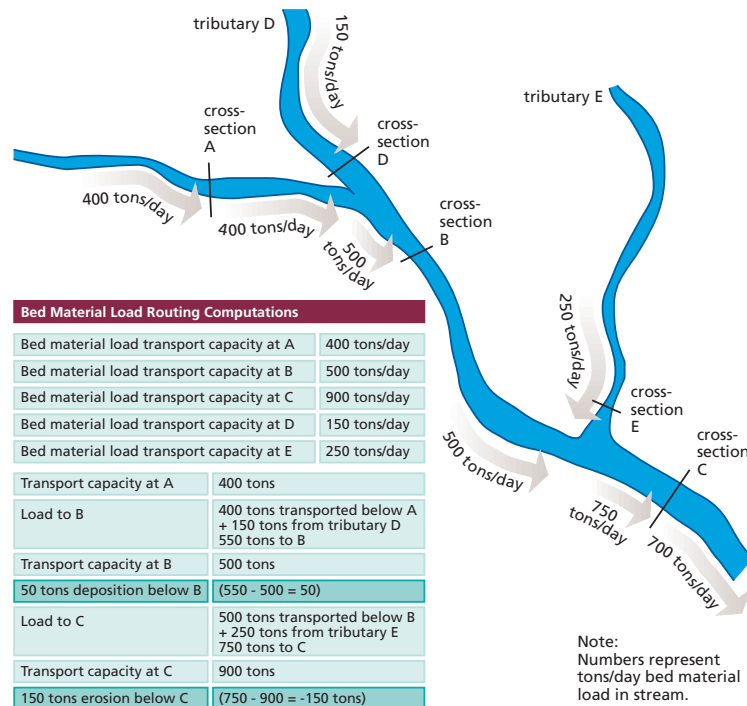An appropriate sediment transport equation is selected, and the transport capacity at each cross section for bed material is computed for the same

Figure 8.35: Sediment budget.
Stream reaches should be evaluated for stability prior to developing a restoration plan.

Bed Material Load Routing Computations	
Bed material load transport capacity at A	400 tons/day
Bed material load transport capacity at B	500 tons/day
Bed material load transport capacity at C	900 tons/day
Bed material load transport capacity at D	150 tons/day
Bed material load transport capacity at E	250 tons/day
Transport capacity at A	400 tons
Load to B	400 tons transported below A + 150 tons from tributary D 550 tons to B
Transport capacity at B	500 tons
50 tons deposition below B	(550 - 500 = 50)
Load to C	500 tons transported below B + 250 tons from tributary E 750 tons to C
Transport capacity at C	900 tons
150 tons erosion below C	(750 - 900 = -150 tons)

Note:
Numbers represent tons/day bed material load in stream.

flow conditions. Figure 8.35 shows the sediment loads in the stream and the transport capacities at each point.

The transport capacities at each point are compared to the sediment load at each point. If the bed material load exceeds the transport capacity, deposition is indicated. If the bed material transport capacity exceeds the coarse sediment load available, erosion of the channel bed or banks is indicated.

Figure 8.35 compares the loads and transport capacities within the reach. The stream might not be stable below B due to deposition. The 50-tons/day deposition is less than 10 percent of the total bed material load in the stream. This small amount of sediment is probably within the area of uncertainty in such analyses. The stream below C probably is unstable due to the excess energy (transport capacity) causing either the banks or bottom to be eroded.

After this type of analysis is complete, the stream should be inspected for areas where sediment is building up or where the stream is eroding. If these problem areas do not match the predictions from the calculations, the sediment transport equation may be inappropriate, or the sediment budget, the hydrology, or the channel surveys may be inaccurate.

Single Storm Versus Average Annual Sediment Discharge

The preceeding example predicts the amount of erosion and deposition that can be expected to occur over one day at one discharge. The bed material transport equation probably used one grain size of sediment. In reality, a variety of flows over varying lengths of time move a variety of sediment particle sizes. Two other approaches should be used to help predict the quantity of bed material sediment

transported by a stream during a single storm event or over a typical runoff year.

To calculate the amount of sediment transported by a stream during a single storm event, the hydrograph for the event is divided into equal-length segments of time. The peak flow or the average discharge for each segment is determined. A spreadsheet can be developed that lists the discharges for each segment of a hydrograph in a column (**Table 8.6**). The transport capacity from the sediment rating curve for each discharge is shown in another column (**Figure 8.36**). Since the transport capacity is in tons/day, a third column should include the length of time represented by each segment of the hydrograph. This column is multiplied by the transport capacity to create a final column that represents the amount of sediment that could be transported over each segment of the hydrograph. Summing the values in

the last column shows the total bed material transport capacity generated by that storm.

Average annual sediment transport in a stream can be determined using a procedure very similar to the storm prediction. The sediment rating curve can be developed from predictive equations or from physical measurements. The annual flow duration curve is substituted for the segmented hydrograph. The same type of spreadsheet described above can be used, and the sum of the values in the last column is the annual sediment-transport capacity (based on predictive equations) or the actual annual sediment transport if the rating curve is based on measured data.

Sediment Discharge After Restoration

After the sediment transport analysis results have been field-checked to ensure that field conditions are accurately predicted, the same analyses are

Table 8.6: Sediment discharges for segments of a hydrograph.

The amount of sediment discharged through a reach varies with time during a stream flow event.

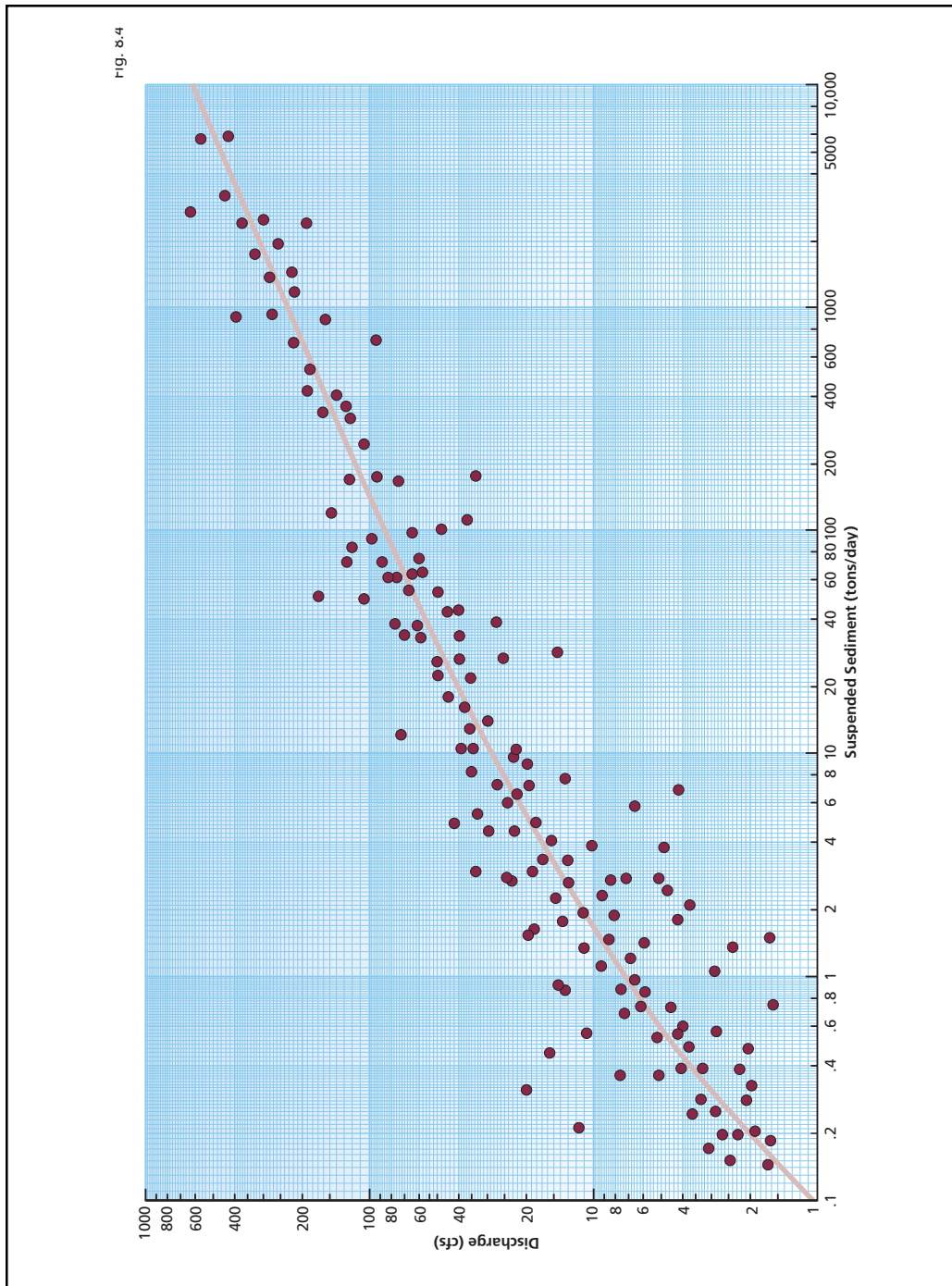| Column 1	Column 2	Column 3	Column 4	Column 5
Segment of Hydrograph	Segment Discharge (ft³/s)	Transport Capacity (tons/day)	Segment Time (days)	Actual Transport (tons)
A	100	150	.42	62
B	280	1700	.42	708
C	483	6000	.42	2500
D	500	6500	.42	2708
E	390	4500	.42	1875
F	155	530	.42	221
G	80	90	.42	38
Total tons transported over the storm				8112
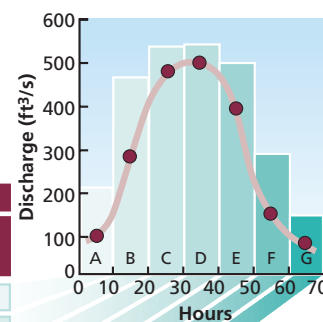
Figure 8.36: Sediment rating curve.
A "sediment rating curve" rates the quantity of sediment carried by a specific stream flow at a defined point or gage.

repeated for the new cross sections and slope in a reconstructed stream or stream reach. Plans and designs may be modified if the second analysis indicates significant deposition or erosion could occur in the modified reach. If potential changes in runoff or sediment yield are predicted to occur in the watershed above a potential restoration site, the sediment transport analyses should be done again based on these potential changes.

Stability Controls

The risk of a restored channel's being damaged or destroyed by erosion or deposition can be reduced if economic considerations permit installation of control measures. Control measures are also required if "natural" levels of channel instability (e.g., meander migration) are unacceptable in the restored reach.

In many cases, control measures double as habitat restoration devices or aesthetic features (Nunnally and Shields 1985, Newbury and Gaboury 1993). Control measures may be categorized as bed stabilization devices, bank stabilization devices, and hydrologic measures. Reviews of control measures are found in Simons and Vanoni (1975), Senturk (1977), Petersen (1986), Chang (1988), and US Army Corps of Engineers (1989b, 1994), and are treated only briefly here. Haan et al. (1994) provide design guidance for sediment control on small watersheds. In all cases, sediment control systems should be planned and designed with the geomorphic evolution of the watershed in mind.

8.F Streambank Restoration

Even where streams retain relatively natural patterns of flow and flooding, stream corridor restoration might require that streambanks be temporarily (years to decades) stabilized while floodplain vegetation recovers. The objective in such instances is to arrest the accelerated erosion often associated with unvegetated banks, and to reduce erosion to rates appropriate for the stream system and setting. In these situations, the initial bank protection may be provided primarily with vegetation, wood, and rock as necessary (refer to *Techniques Appendix*).

In other cases, land development or modified flows may dictate the use of hard structures to ensure permanent stream stability, and vegetation is used primarily to address specific ecological deficiencies such as a lack of channel shading. In either case (permanent or temporary bank stabilization), streamflow projections are used (as described in Chapter 7) to determine the degree to which vegetation must be supplemented with more resistant materials (natural fabrics, wood, rock, etc.) to achieve adequate stabilization.

The causes of excessive erosion may be reversible through changes in land use, livestock management, floodplain restoration, or water management. In some cases, even normal rates of bank erosion and channel movement might be considered unacceptable due to adjacent development, and vegetation might be used primarily to recover some habitat functions in the vicinity

of "hard" bank stabilization measures. In either case, the considerations discussed above with respect to soils, use of native plant species, etc., are applicable within the bank zone. However, a set of specialized techniques can be employed to help ensure plant establishment and improve habitat conditions.

As discussed earlier in this chapter, integration of woody vegetative cuttings, independently or in combination with other natural materials, in streambank erosion control projects is generally referred to as soil bioengineering. Soil-bioengineered bank stabilization systems have not been standardized for general application under particular flow conditions, and the decision as to whether and how to use them requires careful consideration of a variety of factors. On larger streams or where erosion is severe, an effective approach involves a team effort that includes expertise in soils, biology, plant sciences, landscape architecture, geology, engineering, and hydrology.

Soil bioengineering approaches usually employ plant materials in the form of live woody cuttings or poles of readily sprouting species, which are inserted deep into the bank or anchored in various other ways. This serves the dual purposes of resisting washout of plants during the early establishment period, while providing some immediate erosion protection due to the physical resistance of the stems. Plant materials alone are sufficient on some streams or some

Figure 8.37: A stabilized streambank.

Plant materials can be combined with other materials such as rocks, logs or brush, and natural fabrics. [(a) During and (b) after.]

(a)

(b)

bank zones, but as erosive forces increase, they can be combined with other materials such as rocks, logs or brush, and natural fabrics (**Figure 8.37**). In some cases, woody debris is incorporated specifically to improve habitat characteristics of the bank and near-bank channel zones.

Preliminary site investigations (see **Figure 8.38**) and engineering analyses must be completed, as described in Chapter 7, to determine the mode of bank failure and the feasibility of using vegetation as a component of bank stabilization work. In addition to the technical analyses of flows and soils, preliminary investigations must include consideration of access, maintenance, urgency, and availability of materials.

Generalizations regarding water levels and flow velocities should be taken only as indications of the experiences reported from various bank stabilization projects. Any particular site must be evaluated to determine how vegetation can or cannot be used. Soil cohesiveness, the presence of gravel lenses, ice accumulation patterns, the amount of sunlight reaching the bank, and the ability to ensure that grazing will be precluded are all considerations in assessing the suitability of vegetation to achieve bank stabilization. In addition, modified flow patterns may make portions of the bank inhospitable to plants because of inappropriate timing of inundation rather than flow velocities and durations (Klimas 1987). The need to extend protection well beyond the immediate focus of erosion and to protect against flanking is an important design consideration.

As noted in Section 8.E, streambank stabilization techniques can generally be classified as armor, indirect methods, or vegetative methods. The selection of the appropriate stabilization technique is extremely important and can be expressed in terms of the factors discussed below.

Careless Creek, Montana

In the Big Snowy Mountains of central Montana, Careless Creek begins to flow through rangelands and fields until it reaches the Musselshell River. At the beginning of the century, the stream was lined with a riparian cover, primarily of willow. This stream corridor was home to a diversity of wildlife such as pheasant, beaver, and deer.

In the 1930s, a large reservoir was constructed to the west with two outlets, one connected to Careless Creek. These channels were meant to carry irrigation water to the area fields and on to the Musselshell River. Heavy flows during the summer months began to erode the banks (**Figure 8.39a**). In the following years, ranchers began clearing more and more brush for pasture, sometimes burning it out along a stream.

"My Dad carried farmer's matches in his pocket. There was a worn spot on his pants where he would strike a match on his thigh.," said Jessie Zeier, who was raised on a ranch near Careless Creek, recalling how his father often cleared brush.

Any remaining willows or other species were eliminated in the following years as ranchers began spraying riparian areas to control sagebrush. This accelerated the streambank erosion as barren, sometimes vertical, banks began sloughing off chunks of salted gumbo in heavy runoff.

As demand for irrigation water increased downstream, the erosion problem continued. Careless Creek was now carrying not only water, but entire banks, corrals, and fences, as well as tons of silt, and salt from shale deposits, to the Musselshell River. Conflicts between landowners and water users arose over the quantity and quality of the water.

Emotions were running high. Groups began working together to resolve problems. A Technical Advisory Steering Committee was developed to help the planning effort. Many organizations took part, including the Upper and Lower Musselshell Conservation Districts; Natural Resources Conservation Service; Montana Department of Natural Resources and Conservation; Montana Department of Fish; Wildlife and Parks; Deadman's Basin Water Users Association; U.S. Bureau of Reclamation; Central Montana RC&D; City of Roundup; Roundup Sportsmen; county commissioners; and local landowners.

As part of the planning effort, a geographic information system resource inventory was begun in 1993. The inventory revealed about 50 percent of the banks along the 18 miles of Careless Creek were eroding. The inventory helped to locate the areas causing the most problems. Priority was given to headquarters, corrals, and croplands, where stabilization of approximately 5,000 feet of streambank has taken place, funded by EPA monies.

Passive efforts have also begun to stabilize the banks. Irrigation flows in Careless Creek have been decreased for the past 5 years, enabling some areas, such as the one pictured, to begin to self-heal (**Figure 8.39b**). Vegetation has been given a chance to root as erosion has begun to stabilize. Other practices, such as fencing, are being implemented, and future treatments are planned to provide a long-term solution.

Figure 8.39: Careless Creek.
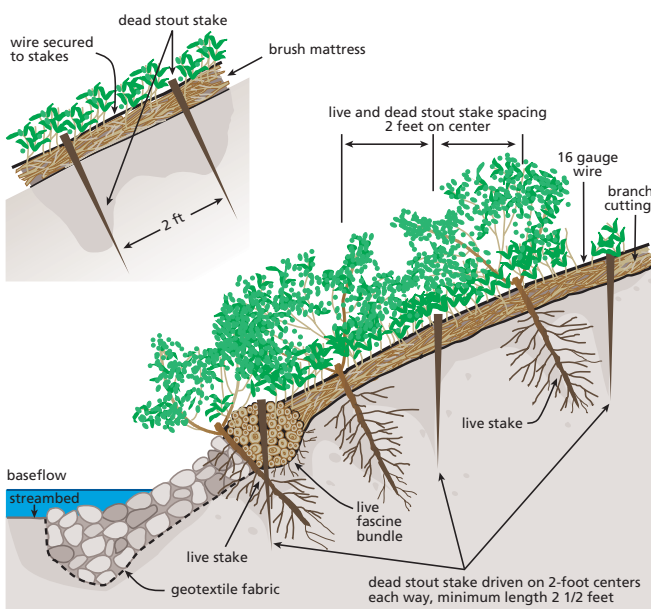*(a) Eroded streambank (May 1995) and (b) streambank in recovery (December 1997).*

(a)

(b)

Figure 8.38: Eroded bank.
Preliminary site investigation and analyses are critical to successful streambank stabilization design.

Figure 8.40: Cutting systems.
Details of brushmattress technique.
Source: Chapter 16 Engineering Handbook, NRCS 1997.

Effectiveness of Technique

The inherent factors in the properties of a given bank stabilization technique, and in the physical characteristics of a proposed work site, influence the suitability of that technique for that site. *Effectiveness* refers to the suitability and adequacy of the technique. Many techniques can be designed to adequately solve a specific bank stability problem by resisting erosive

forces and geotechnical failure. The challenge is to recognize which technique matches the strength of protection against the strength of attack and therefore performs most efficiently when tested by the strongest process of erosion and most critical mechanism of failure. Environmental and economic factors are integrated into the selection procedure, generally making soil bioengineering methods very attractive. The chosen solution, however, must first fulfill the requirement of being effective as bank stabilization; otherwise, environmental and economic attributes will be irrelevant. Soil bioengineering can be a useful tool in controlling streambank erosion, but it should not be considered a panacea. It must be performed in a judicious manner by personnel experienced in channel processes, biology, and streambank stabilization techniques.

Stabilization Techniques

Plants may be established on upper bank and floodplain areas by using traditional techniques for seeding or by planting bare-root and container-grown plants. However, these approaches provide little initial resistance to flows, and plantings may be destroyed if subjected to high water before they are fully established. Cuttings, pole plantings, and live stakes taken from species that sprout readily (e.g., willows) are more resistant to erosion and can be used lower on the bank (**Figure 8.40**). In addition, cuttings and pole plantings can provide immediate moderation of flow velocities if planted at high densities. Often, they can be placed deep enough to maintain contact with adequate soil

Note:
Rooted/leafed condition of the living plant material is not representative at the time of installation.

moisture levels, thereby eliminating the need for irrigation. The reliable sprouting properties, rapid growth, and general availability of cuttings of willows and other pioneer species makes them particularly appropriate for use in bank revegetation projects, and they are used in most of the integrated bank protection approaches described here (see **Figure 8.41**).

Anchored Cutting Systems

Several techniques are available that employ large numbers of cuttings arranged in layers or bundles, which can be secured to streambanks and partially buried. Depending on how these systems are arranged, they can provide direct protection from erosive flows, prevent erosion from upslope water sources, promote trapping of sediments, and quickly develop dense roots and sprouts. Brush mattresses and woven mats are typically used on the face of a bank and consist of cuttings laid side by side and interwoven or pinned down with jute cord or wire held in place by stakes. Brush layers are cuttings laid on terraces dug into the bank, then buried so that the branch ends extend from the bank. Fascines or wattles are bundles of cuttings tied together, placed in shallow trenches arranged horizontally on the bank face, partially buried, and staked in place. A similar system, called a reed roll, uses partially buried and staked burlap rolls filled with soil and root material or rooted shoots to establish herbaceous species in appropriate habitats. Anchored bundles of live cuttings also have been installed perpendicular to the channel on newly constructed gravel floodplain areas to dissipate floodwater energy and

encourage deposition of sediment (Karle and Densmore 1994).

Geotextile Systems

Geotextiles have been used for erosion control on road embankments and other upland settings, usually in combination with seeding, or with plants placed through slits in the fabric (**Figure 8.42**). In self-sustaining streambank applications, only natural, biodegradable materials should be used, such as jute or coconut fiber (Johnson and Stypula 1993). The

Figure 8.41: Results of live staking along a streambank.
Pioneer species are often most appropriate for use in bank revegetation projects.

Figure 8.42: Installation of geotextile.
Geotextile should be made of biodegradable materials such as jute or coconut fibers.

typical streambank use for these materials is in the construction of vegetated geogrids, which are similar to brush layers except that the fill soils between the layers of cuttings are encased in fabric, allowing the bank to be constructed of successive "lifts" of soil, alternating with brush layers. This approach allows reconstruction of a bank and provides considerable erosion resistance (see Green River case study). Natural fibers are also used in "fiber-schines," which are sold specifically for streambank applications. These are cylindrical fiber bundles that can be staked to a bank with cuttings or rooted plants inserted through or into the material.

Vegetated plastic geogrids and other nondegradable materials can also be used where geotechnical problems require drainage or additional strength.

Figure 8.43: Revetment system.
Details of rootwad and boulder technique.
Source: Chapter 16 Engineering Handbook, NRCS 1997.
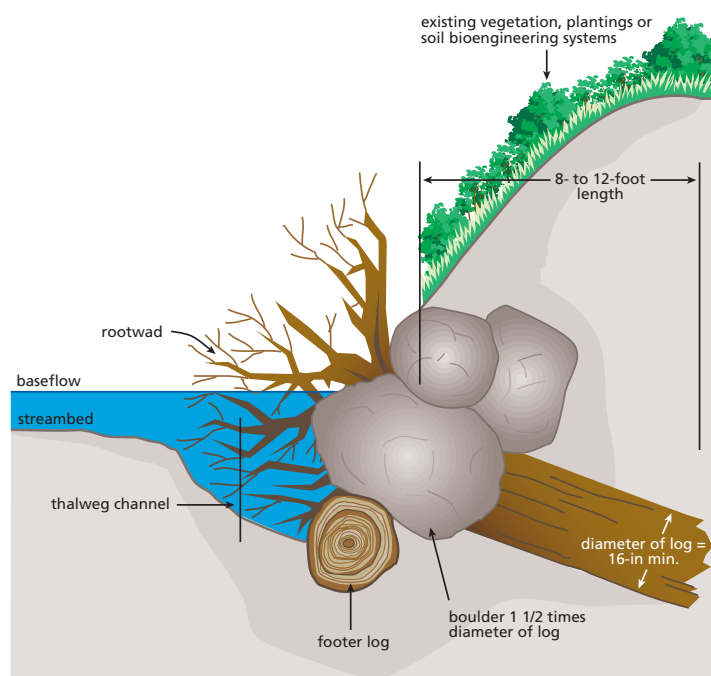
Integrated Systems

A major concern with the use of structural approaches to streambank stabilization is the lack of vegetation in the zone directly adjacent to the water. Despite a long-standing concern that vegetation destabilizes stone revetments, there has been little supporting evidence and even some evidence to the contrary (Shields 1991). Assuming that loss of conveyance is accounted for, the addition of vegetation to structures should be considered. This can involve placement of cuttings during construction, or insertion of cuttings and poles between stones on existing structures. Timber cribwalls may also be constructed with cuttings or rooted plants extending through the timbers from the backfill soils.

Trees and Logs

Tree revetments are made from whole tree trunks laid parallel to the bank, and cabled to piles or deadman anchors. Eastern red cedar (*Juniperus virginiana*) and other coniferous trees are used on small streams, where their springy branches provide interference to flow and trap sediment. The principal objective to these systems is the use of large amounts of cable and the potential for trees to be dislodged and cause downstream damage.

Some projects have successfully used large trees in conjunction with stone to provide bank protection as well as improved aquatic habitat (see case study). Large logs with intact root wads are placed in trenches cut into the bank, such that the root wads extend beyond the bank face at the toe (**Figure 8.43**). The logs are over-

lapped and/or braced with stone to ensure stability, and the protruding rootwads effectively reduce flow velocities at the toe and over a range of flow elevations (**Figure 8.44**). A major advantage of this approach is that it reestablishes one of the natural roles of large woody debris in streams by creating a dynamic near-bank environment that traps organic material and provides colonization substrates for invertebrates and refuge habitats for fish. The logs eventually rot, resulting in a more natural bank. The revetment stabilizes the bank until woody vegetation has matured, at which time the channel can return to a more natural pattern.

In most cases, bank stabilization projects use combinations of the techniques described above in an integrated approach. Toe protection often requires the use of stone, but amounts can be greatly reduced if large logs can also be used. Likewise, stone blankets on the bank face can be replaced with geogrids or supplemented with interstitial plantings. Most upper bank areas can usually be stabilized using vegetation alone, although anchoring systems might be required. The Green River bank restoration case study illustrates one successful application of an integrated approach on a moderate-sized river in Washington State.

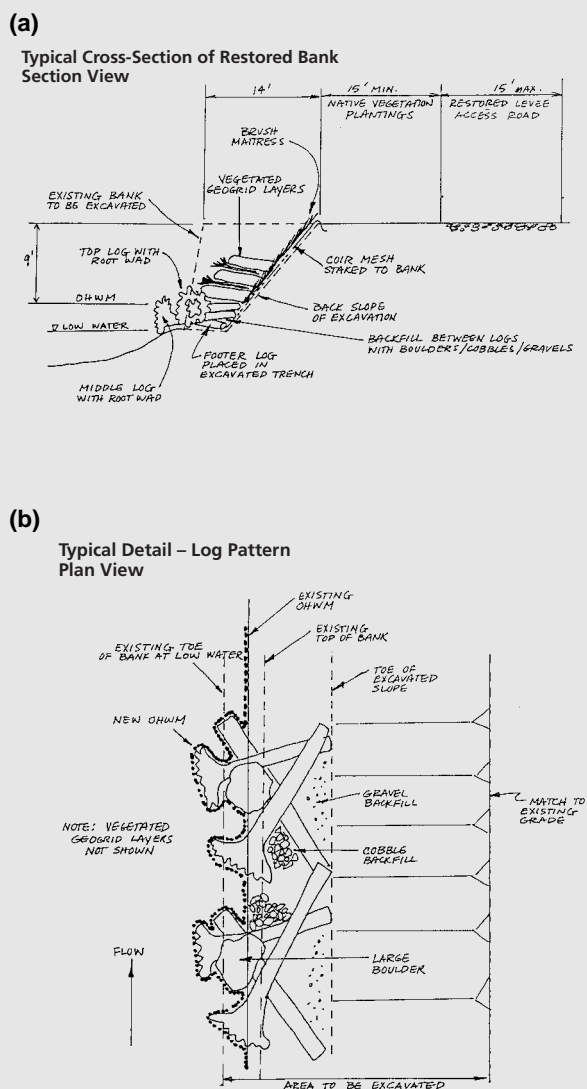**Figure 8.44: Installation of logs with intact root wads.**
An advantage to using tree revetments is the creation of habitat for invertebrates and fish along the streambank.

Green River Bank Restoration Initiative, King County, Washington

The King County, Washington, Surface Water Management Division initiated a bank restoration initiative in 1994 that illustrates a variety of project objectives and soil bioengineering approaches (**Figure 8.45**). The project involved stabilization of the bank of the Green River along a 500-foot section of a meander bend that was rapidly migrating into the adjacent farm field. The project objectives included improvement of fish and wildlife habitat, particularly for salmonids.

Figure 8.45: Construction details.

Source: King County Surface Water Management Division.

(a)

Typical Cross-Section of Restored Bank
Section View

(b)

Typical Detail – Log Pattern
Plan View

Site investigations included surveys of stream cross sections, velocity measurements at two discharge levels, soil characterizations, and assessment of fish use of existing habitat features in the area. The streambank was vertical, 5 to 10 feet high, and composed of silty-clay-loam alluvium with gravel lenses. Flow velocities were 2 to 5 fps for flows of 200 and 550 cfs. Fish were primarily observed in areas of low velocities and/or near woody debris, and along the channel margins.

In August, large woody debris was installed along the toe of the bank. The logs were cedar and fir, 25 feet long and 28 to 36 inches in diameter, with root wads 6 to 8 feet in diameter. The logs were placed in trenches cut 15 feet back into the bank so that the root wads extended into the channel, and large (3- to 4-foot diameter) boulders were placed among the logs at the toe. Log and boulder placement was designed to interlock and brace the logs and prevent movement. The project used approximately 10 logs and 20 boulders per 100 lineal feet of bank. In September, vegetated geogrids were installed above the toe zone to stabilize the high bank **(Figure 8.46)**. The project was completed with installation of a variety of plants, including container-grown conifers and understory species, in a minimum 25-foot buffer along the top of the bank.

Within 2 months of completion, the site was subjected to three high flows, including an 8,430-cfs event in December 1994. Measured velocities along the bank were less than 2 fps at the surface and less than 1 fps 2 feet below the surface, indicating the effectiveness of the root wads in moderating flow velocities **(Figure 8.47)**. Some surface erosion and washout of plants along the top bank occurred, and a subsequent event caused minor damage to the geogrid at one location. The maintenance repairs consisted of replanting and placement of additional logs to halt undermining of the geogrid. The 1995 growing season produced dramatic growth of the willow cuttings in the geogrid, although many of the planted trees in the overbank zone died **(Figure 8.48)**. Initial observations have documented extensive fish use of the slow-water habitats among the root wads at the toe of the bank, and in scour holes created by flows deflected toward the channel bottom.

Figure 8.46: Partially installed vegetated geogrid.
Installed above the toe to stabilize high bank.

The site continues to be carefully monitored, and the effectiveness of the approach has led to the implementation of similar designs elsewhere in the region. The project designers have concluded that future projects of this type should use small plants rather than large rooted material in the overbank zone to reduce costs, improve survival, and minimize damage due to equipment access for maintenance or repair. Based on their observations of fish response along the restored bank and in nearby stream reaches, they also recommend that future projects incorporate a greater variety of woody debris, including brushy material and tree tops, along the toe and lower bank.

Figure 8.47: Completed system.
Note calm water along bankline during high flow.

Figure 8.48: Completed system after one year.
Note dramatic willow growth from vegetated geogrid.

8.G Instream Habitat Recovery

As described in Chapter 2, habitat is the place where a population lives and includes living and nonliving components. For example, fish habitat is a place, or set of places, in which a single fish, a population, or an assemblage of fish can find the physical, chemical, and biological features needed for life, including suitable water quality, passage routes, spawning grounds, feeding and resting sites, and shelter from predators and adverse conditions (**Figure 8.49**). Principal factors controlling the quality of the available aquatic habitat include:

- Streamflow conditions.

- Physical structure of the channel.

- Water quality (e.g., temperature, pH, dissolved oxygen, turbidity, nutrients, alkalinity).

- The riparian zone.

- Other living components.

The existing status of aquatic habitats within the stream corridor should be assessed during the planning stage (Part II). Design of channels, structures, or restoration features can be guided and fine tuned by assessing the quality and quantity of habitats provided by the proposed design. Additional guidance on assessing the quantity and quality of aquatic habitat is provided in Chapter 7.

This section discusses the design of instream habitat structures for the purpose of enhancing physical aquatic habitat quality and quantity. It should be noted, however, that the best approach to habitat recovery is to restore a fully functional, well-vegetated stream corridor within a well-managed

Figure 8.49: Instream habitat.
Suitable water quality, passage routes, and spawning grounds are some of the characteristics of fish habitat.

Man-made structures are less sustainable and rarely as effective as a stable channel.

watershed. Man-made structures are less sustainable and rarely as effective as a stable channel. Over the long term, design should rely on natural fluvial processes interacting with floodplain vegetation and associated woody debris to provide high-quality aquatic habitat. Structures have little effect on populations that are limited by factors other than physical habitat.

Instream Habitat Features

The following procedures to restore instream habitat are adapted from Newbury and Gaboury (1993) and Garcia (1995).

- *Select stream.* Give priority to reaches with the greatest difference between actual (low) and potential (high) fish carrying capacity and with a high capacity for natural recovery processes.

- *Evaluate fish populations and their habitats.* Give priority to reaches with habitats and species of special interest. Is this a biological, chemical, or physical problem? If a physical problem:

Figure 8.50: Surveying a stream.
Channel surveys establish baseline information needed for restoration design.

- *Diagnose physical habitat problems.*

  -Drainage basin. Trace water-shed lines on topographical and geological maps to identify sample and rehabilitation basins.

  -Profiles. Sketch main stem and tributary long profiles to identify discontinuities that might cause abrupt changes in stream characteristics (falls, former base levels, etc.).

  -Flow. Prepare flow summary for rehabilitation reach using existing or nearby records if available (flood frequency, minimum flows, historical mass curve). Correct for drainage area differences. Compare magnitude and duration of flows during spawning and incubation to year class strength data to determine minimum and maximum flows required for successful reproduction.

  -Channel geometry survey. Select and survey sample reaches to establish the rela-tionship between channel geometry, drainage area, and bankfull channel-forming discharge (**Figure 8.50**). Quantify hydraulic parameters at design discharge.

  -Rehabilitation reach survey. Survey rehabilitation reaches in sufficient detail to prepare channel cross section profiles and construction drawings and to establish survey reference markers.

-Preferred habitat. Prepare a summary of habitat factors for biologically preferred reaches using regional references and surveys. Identify multiple limiting factors for the species and life stages of greatest concern. Where possible, undertake reach surveys in reference streams with proven populations to identify local flow conditions, substrate, refugia, etc.

• *Design a habitat improvement plan.* Quantify the desired results in terms of hydraulic changes, habitat improvement, and population increases. Integrate selection and sizing of rehabilitation works with instream flow requirements.

-Select potential schemes and structures that will be reinforced by the existing stream dynamics and geometry. The following section provides additional detail on use of habitat structures.

-Test designs for minimum and maximum flows and set target flows for critical periods derived from the historical mass curve.

• *Implement planned measures.*

-Arrange for on-site location and elevation surveys and provide advice for finishing details in the stream.

• *Monitor and evaluate results.*

-Arrange for periodic surveys of the rehabilitated reach and reference reaches, to improve the design, as the channel ages.

Instream Habitat Structures

Aquatic habitat structures (also called instream structures and stream improvement structures) are widely used in stream corridor restoration. Common types include weirs, dikes, random rocks, bank covers, substrate reinstatement, fish passage structures, and off-channel ponds and coves. Institutional factors have favored their use over more holistic approaches to restoration. For example, it is often easier to obtain authority and funding to work within a channel than to influence riparian or watershed land use. Habitat structures have been used more along cold water streams supporting salmonid fisheries than along warm water streams, and the voluminous literature is heavily weighted toward cold water streams.

In a 1995 study entitled *Stream Habitat Improvement Evaluation Project,* 1,234 structures were evaluated according to their general effectiveness, the habitat quality associated with the given structure type, and actual use of the structures by fish (Bio West 1995). The study determined approximately 18 percent of the structures need maintenance. Where inadequate flows and excessive sediment delivery occur, structures have a brief lifespan and limited value in terms of habitat improvement. Furthermore, the study concluded that instream habitat structures generally provided increased fish habitat.

Before structural habitat features are added to a stream corridor restoration design, project managers should carefully determine whether they address the real need and are appropriate. Major caveats include the following:
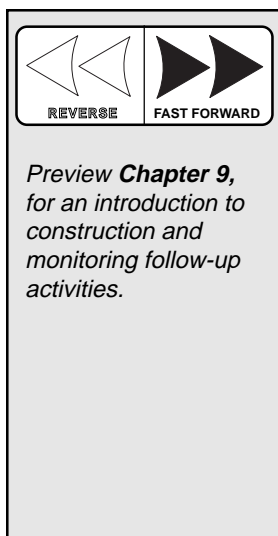
- Structures should never be viewed as a substitute for good riparian and upland management.

- Defining the ecological purpose of a structure and site selection are as important as construction technique.

- Scour and deposition are natural stream processes necessary to create fish habitat. Overstabilization therefore limits habitat potential, whereas properly designed and sited structures can speed ecological recovery.

- Use of native materials (stone and wood) is strongly encouraged.

- Periodic maintenance of structures will be necessary and must be incorporated into project planning.

Instream Habitat Structure Design

Design of aquatic habitat structures should proceed following the steps presented below (Shields 1983). However, the process should be viewed as iterative, and considerable recycling among steps should be expected.

- Plan layout.
- Select types of structures.
- Size the structures.
- Investigate hydraulic effects.
- Consider effects on sediment transport.
- Select materials and design structures.

Each step is described below. Construction and monitoring follow-up activities are described in Chapter 9.

Plan Layout

The location of each structure should be selected. Avoid conflicts with bridges, riparian structures, and existing habitat resources (e.g., stands of woody vegetation). The frequency of structures should be based on the habitat requirements previously determined, within the context of the stream morphology and physical characteristics (see Chapter 7). Care should be taken to place structures where they will be in the water during baseflow. Structures should be spaced to avoid large areas of uniform conditions. Structures that create pools should be spaced five to seven channel widths apart. Weirs placed in series should be spaced and sized carefully to avoid placing a weir within the backwater zone of the downstream structure, since this would create a series of pools with no intervening riffles or shallows.

Select Types of Structures

The main types of habitat structures are weirs, dikes (also called jetties, barbs, deflectors (**Figure 8.51**), spurs, etc.), random rocks (also called boulders), and bank covers (also called lunkers). Substrate reinstatement (artificial riffles), fish passage structures, and off-channel ponds and coves have also been widely employed. Fact sheets on several of these techniques are provided in the Techniques Appendix, and numerous design web sites are available (White and Brynildson 1967, Seehorn 1985, Wesche 1985,

Orsborn et al. 1992, Orth and White 1993, Flosi and Reynolds 1994).

Evidence suggests that traditional design criteria for widespread bank and bed stabilization measures (e.g., concrete grade control structures, homogeneous riprap) can be modified, with no functional loss, to better meet environmental objectives and improve habitat diversity. **Table 8.8** may be used as a general guide to relate structural type to habitat requirement. Weirs are generally more failure-prone than deflectors. Deflectors and random rocks are minimally effective in environments where higher flows do not produce sufficient local velocities to produce scour holes near structures. Random rocks (boulders) are especially susceptible to undermining and burial when placed in sand-bed channels, although all types of stone structures experience similar problems. Additional guidance for evaluating the general suitability of various fish habitat structures for a wide range of morphological stream types is provided by Rosgen (1996). Seehorn (1985) provides guidance for small streams in the eastern United States. The use of any of these guides should also consider the relative stability of the stream, including aggradation and incision trends, for final design.

Size the Structures

Structures should be sized to produce the desired aquatic habitats at the normal range of flows from baseflow to bankfull discharge. A hydrological analysis can provide an estimate of the normal range of flows (e.g., a flow duration curve), as well as an estimate
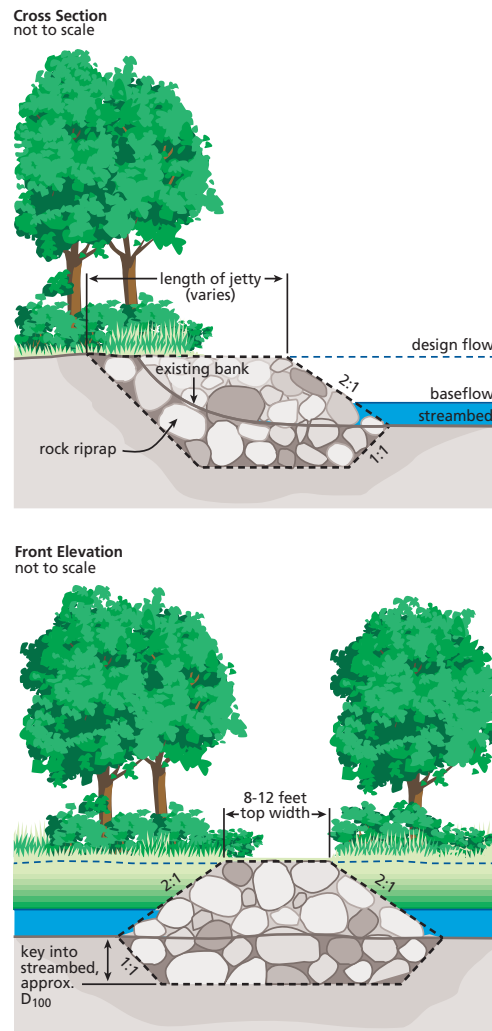
Figure 8.51: Instream habitat structure.
Wing deflector habitat structure.
Source: Chapter 16 Engineering Handbook, NRCS 1997.

of extreme high and low flows that might be expected at the site (see Chapter 7). In general, structures should be low enough that their effects on the water surface profile will be slight at bankfull discharge. Detailed guidance by structural type is presented in the *Techniques Appendix*. For informal design, empirical equations like those presented by Heiner (1991) can be used to roughly estimate the depth of scour holes at weirs and dikes.

Table 8.9: Fish habitat improvement structures —suitability for stream types.
From Rosgen 1996

Channel Type	Low St. Check Dam	Medium St. Check Dam	Boulder Placement	Bank Boulder Placement	Single Wing Deflector	Double Wing Deflector	Channel Constrictor	Bank Cover
A1	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
A2	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
B1-1	Poor	Poor	Good	Excellent	Poor	Poor	Poor	Good
B1	Excellent	Excellent	N/A	N/A	Excellent	Excellent	N/A	Excellent
B2	Excellent	Good	Excellent	Excellent	Excellent	Excellent	Excellent	Excellent
B3	Fair	Poor	Poor	Good	Poor	Poor	Poor	Poor
B4	Fair	Poor	Poor	Good	Poor	Poor	Poor	Poor
B5	Fair	Poor	Poor	Good	Poor	Poor	Poor	Poor
C1-1	Poor	Poor	Fair	Excellent	Poor	Poor	Poor	Good
C1	Good	Fair	Fair	Excellent	Good	Good	Fair	Good
C2	Excellent	Good	Good	Excellent	Good	Excellent	Excellent	Good
C3	Fair	Poor	Poor	Good	Fair	Fair	Fair	Good
C4	Fair	Poor	Poor	Good	Poor	Poor	Poor	Fair
C5	Fair	Poor	Poor	Good	Poor	Poor	Poor	Poor
C6	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
D1	Fair	Poor	Poor	Fair	Fair	Fair	Fair	Poor
D2	Fair	Poor	Poor	Fair	Fair	Fair	Fair	Poor

Channel Type	Half Log Cover	Floating Log Cover	Submerged Shelter		Migration Barrier	Gravel Traps		Gravel Placement
			Meander	Straight		"V" Shaped	Log	
A1	N/A	N/A	N/A	N/A	Excellent	Good	Poor	Poor
A2	N/A	N/A	N/A	N/A	Excellent	Excellent	Excellent	Poor
B1-1	Good	Good	Good	Excellent	Fair	Good	Good	Fair
B1	Good	Excellent	Excellent	Excellent	Excellent	Excellent	Excellent	Fair
B2	Excellent	Excellent	Good	Excellent	Good	Good	Good	Good
B3	Poor	Fair	Fair	Fair	Poor	Poor	Poor	Poor
B4	Poor	Fair	Fair	Fair	Poor	Poor	Poor	Poor
B5	Poor	Fair	Fair	Fair	Poor	Poor	Poor	Poor
C1-1	Good	Good	Good	Excellent	Poor	Fair	Fair	Fair
C1	Good	Good	Good	Excellent	Poor	Fair	Good	Fair
C2	Good	Excellent	Excellent	Excellent	Poor	Good	Excellent	Excellent
C3	Fair	Good	Fair	Good	Poor	N/A	N/A	N/A
C4	Poor	Good	Fair	Good	Poor	Poor	Poor	Poor
C5	Poor	Good	Fair	Good	Poor	Poor	Poor	Poor
C6	N/A	N/A	N/A	N/A	Poor	Poor	Fair	Fair
D1	Poor	Poor	Poor	Poor	Poor	Poor	N/A	Poor
D2	Poor	Poor	Poor	Poor	Poor	N/A	Poor	Poor

Key:
Excellent   - No limitation to location of structure placement or special modification in design.
Good   - Under most conditions, very effective. Minor modification of design or placement required.
Fair   - Serious limitation which can be overcome by placement location, design modification or stabilization techniques.
          Generally not recommended due to difficulty of offsetting potential adverse consequences and high probability of reduced effectiveness.
Poor   - Not recommended due to morphological character of stream type and very low probability of success.
Not Applicable- Generally not considered since habitat components are not limiting.
Note : A3, A3-a, A4, A4-a, A5, A5-a channel types are not evaluated due to limited fisheries value.

Investigate Hydraulic Effects

Hydraulic conditions at the design flow should provide the desired habitat; however, performance should also be evaluated at higher and lower flows. Barriers to movement, such as extremely shallow reaches or vertical drops not submerged at higher flows, should be avoided. If the conveyance of the channel is an issue, the effect of the proposed structures on stages at high flow should be investigated. Structures may be included in a standard backwater calculation model as contractions, low weirs, or increased flow resistance (Manning) coefficients, but the amount of increase is a matter of judgment or limited by National Flood Insurance Program ordinances. Scour holes should be included in the channel geometry downstream of weirs and dike since a major portion of the head loss occurs in the scour hole. Hydraulic analysis should include estimation or computation of velocities or shear stresses to be experienced by the structure.

Consider Effects on Sediment Transport

If the hydraulic analysis indicates a shift in the stage-discharge relationship, the sediment rating curve of the restored reach may change also, leading to deposition or erosion. Although modeling analyses are usually not cost-effective for a habitat structure design effort, informal analyses based on assumed relationships between velocity and sediment discharge at the bankfull discharge may be helpful in detecting potential problems. An effort should be made to predict the locations and magnitude of local scour and deposition. Areas projected to experience significant scour and deposition should be prime sites for visual monitoring after construction.

Select Materials

Materials used for aquatic habitat structures include stone, fencing wire, posts, and felled trees. Priority should be given to materials that occur on site under natural conditions. In some cases, it may be possible to salvage rock or logs generated from construction of channels or other project features. Logs give long service if continuously submerged. Even logs not continuously wet can give several decades of service if chosen from decay-resistant species. Logs and timbers must be firmly fastened together with bolts or rebar and must be well anchored to banks and bed. Stone size should be selected based on design velocities or shear stress.

8.H Land Use Scenarios

As discussed in Chapter 3, most stream corridor degradation is directly attributable to land use practices and/or hydrologic modifications at the watershed level that cause fundamental disruption of ecosystem functions (Beschta et al. 1994) (**Figure 8.52**). Ironically, land use practices, including hydrologic modifications, can offer the opportunity for restoring these same degraded stream corridors. Where feasible, the objective of the restoration design should be to eliminate or moderate disruptive influences sufficiently to allow recovery of dynamic equilibrium over time (NRC 1992).

If chronic land use impacts on the stream or riparian system cannot be controlled or moderated, or if some elements of the stream network (e.g., headwaters) are not included in the restoration design, it must be recognized that the restoration action may have limited effectiveness in the long-term.

Restoration measures can be designed to address particular, site-specific deficiencies (an eroding bank, habitat features), but if they do not restore self-maintaining processes and the functions of a stream corridor, they must be regarded as a focused "fix" rather than an ecosystem restoration. In cases where land use practices are the direct cause of stream corridor degradation and there is a continuing downward trend in landscape condition, there is little point in expending resources to address symptoms of the

problem rather than the problem itself (DeBano and Schmidt 1989).

Design Approaches for Common Effects

Agriculture, forestry, grazing, mining, recreation, and urbanization are some of the principal land uses that can result in disturbance of stream corridor structure and functions. A watershed analysis will help prioritize and coordinate restoration actions (Platts and Rinne 1985, Swanson 1989) and may indicate critical or chronic land use activities causing disturbance both inside and outside the stream corridor. Addressing these in the restoration plan and design, may greatly improve the effectiveness and success of restoration work.

Restoration measures designed in response to these effects may be similar across land uses. Sediment and nutrient management in urban, agricultural, and forest settings, for

Figure 8.52: Sediment-laden stream.
Most stream corridor degradation can be attributed to impacts resulting from surrounding land uses.

instance, may require the use of buffer strips. Although the buffer strips have many common design characteristics, each setting has site-specific factors.

Dams

Dams alter the flow of water, sediment, organic matter, and nutrients, resulting in both direct physical and indirect biological effects in tailwaters and downstream riparian and floodplain areas (see Chapter 3). Stream corridors below dams can be partially restored by modifying operation and management approaches. Impacts from the operation of dams on surface water quality and aquatic and riparian habitat should be assessed and the potential for improvement evaluated. The modification of operation approaches, where possible, in combination with the application of properly designed and applied best management practices, can reduce the impacts caused by dams on downstream riparian and floodplain habitats.

Best management practices can be applied individually or in combination to protect and improve surface water quality and aquatic habitat in reservoirs as well as downstream. Several approaches have been designed for improving or maintaining acceptable levels of dissolved oxygen (DO), temperature, and other constituents in reservoirs and tailwaters. One design approach uses pumps, air diffusers, or air lifts to induce circulation and mixing of the oxygen-poor but cold hypolimnion with the oxygen-rich but warm epilimnion, resulting in a more thermally uniform reservoir with increased DO. Another design approach for improving water quality in

tailwaters for trout fisheries involves mixing of air or oxygen with water passing through the turbines at hydropower dams to improve concentrations of DO. Reservoir waters can also be aerated by venting turbines to the atmosphere or by injecting compressed air into the turbine chamber (USEPA 1993).

Modification to the intakes, the spillway, or the tailrace of a dam can also be designed to improve temperature or DO levels in tailwaters. Installing various types of weirs downstream of a dam achieves similar results. These design practices rely on agitation and turbulence to mix reservoir releases with atmospheric air to increase levels of DO (USEPA 1993).

Adequate fish passage around dams, diversions, and other obstructions may be a critically important component of restoring healthy fish populations to previously degraded rivers and streams. A fact sheet in Appendix A shows an example for fish passages. However, designing, installing, and operating fish passage facilities at dams are beyond the scope of this handbook. Further, the type of fish passage facility and the flows necessary for operation are generally site specific. Further information on fish passage technology can be found in other references, including *Environmental Mitigation at Hydroelectric Projects - Volume II. Benefits and Costs of Fish Passage and Protection* (Francfort et al., 1994); and *Fish Passage Technologies: Protection at Hydropower Facilities* (Office of Technology Assessment, Congress of the United State, Washington DC, OTA-ENV-641).

Adjusting operation procedures at some dams can also result in improved quality of reservoir releases and downstream conditions. Partial restoration of stream corridors below dams can be achieved by designing operation procedures that mimic the natural hydrograph, or desirable aspects of the hydrograph. Modifications include scheduling releases or the duration of shutoff periods, instituting procedures for the maintenance of minimum flows, and making seasonal adjustments in pool levels and in the timing and variation of the rates of drawdowns (USEPA 1993).

Modifying operation and management approaches, in combination with the application of properly designed best management practices, can be an effective approach to partially restoring stream corridors below dams. However, dam removal is the only way to begin to fully restore a stream to its natural condition. It is important to note, however, that unless accomplished very carefully, with sufficient studies and modeling and at significant cost, removing a dam can cause more damage downstream (and upstream) than the dam is currently causing until a state of dynamic equilibrium is reached. Dam removal lowers the base level of upstream tributaries, which can cause rejuvenation, bed and bank instability, and increased sediment loads. Dam removal can also result in the loss of wetlands and habitat in the reservoir and tributary deltas.

Three options should be considered— complete removal, partial removal, and staged breaching. The option is selected based on the condition of the

dam and future maintenance required if not completely removed, and on the best way to deal with the sediment now stored behind the dam. The following elements must be considered in managing sediment:

- Removing features of dams necessary to restore fish passage and ensure safety.
- Revegetation of the reservoir areas.
- Long-term monitoring of sediment transport and river channel topography, water quality, and aquatic ecology.
- Long-term protection of municipal and industrial water supplies.
- Mitigation of flood impacts caused by long-term river aggradation.
- Quality of sediment, including identification of the lateral and vertical occurrence of toxic or otherwise poor-quality sediment.

Water quality issues are primarily related to suspended sediment concentration and turbidity. These are important to municipal, industrial, and private water users, as well as to aquatic communities. Water quality will primarily be affected by any silt and clay released from the reservoirs and by reestablishment of the natural sediment loads downstream. During removal of the dam and draining of the lake, the unvegetated reservoir bottoms will be exposed. Lakebeds will be expected to have large woody debris and other organic material. A revegetation program is necessary to control dust, surface runoff, and

erosion and to restore habitat and aesthetic values. A comprehensive sediment management plan is needed to address the following:

- Sediment volume and physical properties.
- Sediment quality and associated disposal requirements.
- Hydraulic and biological characteristics of the reservoir and downstream channel.
- Alternative measures for sediment management.
- Impacts on downstream environment and channel hydraulics.
- Recommended measures to manage sediment properly and economically.

Objectives of sediment management should include flood control, water quality, wetlands, fisheries, habitat, and riparian rights.

For hydropower dams, the simplest decommissioning program is to dismantle the turbine-generator and seal the water passages, leaving the dam and water-retaining structures in place. No action is taken concerning the sediments since they will remain in the reservoir and the hydraulic and physical characteristics of the river and reservoir will remain essentially unchanged. This approach is viable only if there are no deficiencies in the water-retaining structures (such as inadequate spillway capacity or inadequate factors of safety for stability) and long-term maintenance is ensured. In some cases, decommissioning can include partial removal of water-retaining structures. Partial removal involves demolition of a portion of the

dam to create a breach so that it no longer functions as a water-retaining structure.

For additional information, see *Guidelines for the Retirement of Hydroelectric Facilities* published by the American Society of Civil Engineers (ASCE) in 1997.

Channelization and Diversions

Channelization and flow diversions represent forms of hydrologic modification commonly associated with most principal land uses, and their effects should be considered in all restoration efforts (see Chapter 3). In some cases, restoration design can include the removal or redesign of channel modifications to restore preexisting ecological and flow characteristics.

Modifications of existing projects, including operation and maintenance or management, can improve some negative effects without changing the existing benefits or creating additional problems. Levees may be set back from the stream channel to better define the stream corridor and reestablish some or all of the natural floodplain functions. Setback levees can be constructed to allow for overbank flooding, which provides surface water contact with streamside areas such as floodplains and wetlands.

Instream modifications such as uniform cross sections or armoring associated with channelization or flow diversions may be removed, and design and placement of meanders can be used to reestablish more natural channel characteristics. In many cases, however, existing land uses might limit or prevent the removal of existing channel or floodplain modifi-

cations. In such cases, restoration design must consider the effects of existing channel modifications or flow diversions, in the corridor and the watershed.

Exotic Species

Exotic species are another common problem of stream corridor restoration and management. Some land uses have actually introduced exotics that have become uncontrolled, while others have merely created an opportunity for such exotics to spread. Again, control of exotic species has some common aspects across land uses, but design approaches are different for each land use.

Control of exotics in some situations can be extremely difficult and may be impractical if large acreages or well-established populations are involved. Use of herbicides may be tightly regulated or precluded in many wetland and streamside environments, and for some exotic species there are no effective control measures that can be easily implemented over large areas (Rieger and Kreager 1988). Where aggressive exotics are present, every effort should be made to avoid unnecessary soil disturbance or disruption of intact native vegetation, and newly established populations of exotics should be eradicated.

Nonnative species such as salt cedar (*Tamarix* spp.) and Russian olive (*Elaeagnus angustifolia*) can outcompete native plantings and negatively affect their establishment and growth. The likelihood of successful reestablishment often increases when artificial flows created by impoundments are altered to favor native species and when exotics such as salt cedar are removed before revegetation is attempted (Briggs et al. 1994).

Salt cedar is an aggressive, exotic colonizer in the West due to its long period and high rate of seed production, as well as its ability to withstand long periods of inundation. Salt cedar can be controlled either by clearing with a bulldozer or by direct application of herbicide (Sudbrock 1993); however, improper treatments may actually increase the density of salt cedar (Neill 1990).

Controlling exotics and weeds can be important because of potential competition with established native vegetation, colonized vegetation, and artificially planted vegetation in restoration work. Exotics compete for moisture, nutrients, sunlight, and space and can adversely influence establishment rates of new plantings. To improve the effectiveness of revegetation work, exotic vegetation should be cleared prior to planting; nonnative growth must also be controlled after planting. General techniques for control of exotics and weeds are mechanical (e.g., scalping or tilling), chemical (herbicides), and fire. For a review of treatment methods and equipment, see U.S. Forest Service (1965) and Yoakum et al. (1980).

Agriculture

America's Private Land—A Geography of Hope (NRCS 1997) challenges all of us to "regain our sense of place and renew our commitment to private landowners and the public." It suggests that as we learn more about the complexity of our environment,

The Multispecies Riparian Buffer System in the Bear Creek, IA Watershed

Introduction

The Bear Creek Watershed in central Iowa is a small (26.8 mi^2) drainage basin located within the Des Moines Lobe subregion of the Western Corn Belt Plains ecoregion, one of the youngest and flattest ecological subregions in Iowa. In general, the land is level to gently rolling with a poorly developed stream network. Soils of the region are primarily developed in glacial till and alluvial, lacustrine, and windblown deposits. Prior to European settlement of the region (*ca* 1847) the watershed consisted of the vast tallgrass prairie ecosystem, interspersed with wet prairie marshes in topographic lows and gallery forests along larger order streams and rivers. Native forest was limited to the Skunk River corridor into which Bear Creek flows.

Subsequent conversion of the land, including the riparian zone, from native vegetation to row crops, extensive subsurface drainage tile installation, dredge ditching and grazing of fenced riparian zones have resulted in substantial stream channel modification. Records suggest that artificial drainage of marshes and low prairies in the upper reaches of the Bear Creek watershed was completed about 1902, with ditch dredging completed shortly thereafter. While the main stream pattern appears to have remained about the same since that time, significant channelization continued into the 1970s. Additional intermittent channels have developed in association with new drainage tile and grass waterway installation. Present land use in the Bear Creek watershed is typical of the region with over 87% of the land area devoted to row crop agriculture.

Landscape modifications and present land-use practices have produced nonpoint source pollution in the watershed which landowners have addressed by implementing soil conservation practices (e.g. reduced tillage, terracing, grass waterways) and better chemical input management (e.g. more accurate and better timed applications). It has only been recently that placement or enhancement of riparian vegetation or "streamside filter strips" has been recommended to reduce sediment and chemical loading, modify flow regime by reducing discharge extremes, improve structural habitat, and restore energy relationships through the addition of organic matter and reduction in temperature and dissolved oxygen extremes.

The Riparian Management System (RiMS)

The Agroecology Issue Team of the Leopold Center for Sustainable Agriculture, Iowa State University, Ames, IA, is conducting research on the design and establishment of an integrated riparian management system (RiMS) to demonstrate the benefits of properly functioning riparian buffers in the heavily row-cropped landscape of the midwestern U.S.. The purpose of the RiMS is to restore the essential ecological functions that riparian ecosystems once provided. Specific objectives of such buffers are to intercept eroding soil and agricultural chemicals from adjacent crop fields, slow floodwaters, stabilize streambanks, provide wildlife habitat, and improve the biological integrity of aquatic ecosystems. The regionalization of this system has been accomplished by designing it with several components, each of which can be modified to fit local landscape conditions and landowner objectives.

The Agroecology Issue Team is conducting detailed studies of important biological and physical processes at both the field and watershed scale to provide the necessary data to allow resource managers to make credible recommendations of buffer placement and design in a wide variety of landscapes. In addition, socioeconomic data collected from landowners in the watershed are being used to identify landowner criteria for accepting RiMS. The team also is quantifying the non-market value placed on the improvement in surface and ground water quality.

The actual development and establishment of the RiMS along Bear Creek was initiated in 1990 along a 0.6 mile length of Bear Creek on the Ron and Sandy Risdal Farm. The buffer strip system has subsequently been planted along 3.5 miles of Bear Creek upstream from this original site. The RiMS consists of three components: 1) a multi-species riparian buffer (MRB), 2) soil bioengineering technologies for streambank stabilization, and 3) constructed wetlands to intercept and process nonpoint source pollutants in agricultural drainage tile water.

Multi-species Riparian Buffer (MRB)

The general MRB consists of three zones. The rapid growth of this buffer community can change a heavily impacted riparian zone into a functioning riparian ecosystem in a few short years. The combinations of trees, shrubs and native grasses can be modified to fit site conditions (e.g. soils, slope), major buffer biological and physical function(s), owner objectives, and cost-share program requirements.

Soil Bioengineering

It has been estimated that greater than 50% of the stream sediment load in small watersheds in the Midwest is the result of channel erosion. This problem has been worsened by the increased erosive power of streams resulting from stream channelization and loss of riparian vegetation. Several different soil bioengineering techniques have been employed in the Bear Creek watershed. These include the use of willow posts and stakes driven into the bank, live willow fascines, live willow brush mattresses and biodegradable geotextile anchored with willow stakes on bare slopes. Alternatives used to stabilize the base of the streambank include rock and anchored dead plant material such as cedar or bundled maple.

Constructed Wetlands

Small, constructed wetlands which are integrated into the riparian buffer have considerable potential to remove nitrate and other chemicals from the extensive network of drain tile in the midwest. To demonstrate this technology, a small (600 yd^2) wetland was constructed to process drainage tile water from a 12 acre cropped field. The wetland was constructed by excavating a depressional area near the creek and constructing a low berm. The subsurface drainage tile was rerouted to enter the wetland at a point that maximizes residence time of drainage tile water within the wetland. A simple gated water level control structure at the wetland outlet provides control of the water level maintained within the wetland. Cattail rhizomes *(Typha glauca* Godr.*)* collected from a local marsh and road ditch were planted within the wetland and native grasses and forbs planted on the constructed berm. Future plans include the construction of additional tile drainage wetlands within the Bear Creek watershed.

System Effectiveness

Long-term monitoring has demonstrated the significant capability of the RiMS to intercept eroding soil from adjacent cropland, intercept and process agricultural chemicals moving in shallow subsurface water, stabilize stream channel movement, and improve instream environments, while also providing wildlife habitat, and quality timber products. The buffer traps between 70-80% of the sediment carried in surface runoff and has reduced nitrate and atrazine moving in the soil solution to levels well below the maximum contaminant levels specified by the USEPA. Streambank bioengineering systems have virtually stopped bank erosion along treated reaches and are now trapping channel sediment. The constructed wetland has reduced nitrate in the tile drainage water by as much as 80% depending on the season of the year. Wildlife benefits have also appeared in a very short time with a nearly five fold increase in bird species diversity observed within the buffer strip versus an adjacent, unprotected stream reach.

While the RiMS function is being assessed through experimental plot work with intensive process monitoring economic benefits and costs to landowners and society also are being determined. Landowners surveys, focus groups, and one-on-one interviews have identified the concern that water quality should be improved by reducing chemical and sediment inputs by as much as 50%. Landowners are willing to pay for this improved water quality as well as volunteer their time to help initiate the improvements.

While the RiMS can effectively intercept and treat nonpoint source pollution from the uplands it should be stressed that a riparian management system cannot replace upland conservation practices. In a properly functioning agricultural landscape, both upland conservation practices and an integrated riparian system contribute to achieving environmental goals and improved ecosystem functioning.
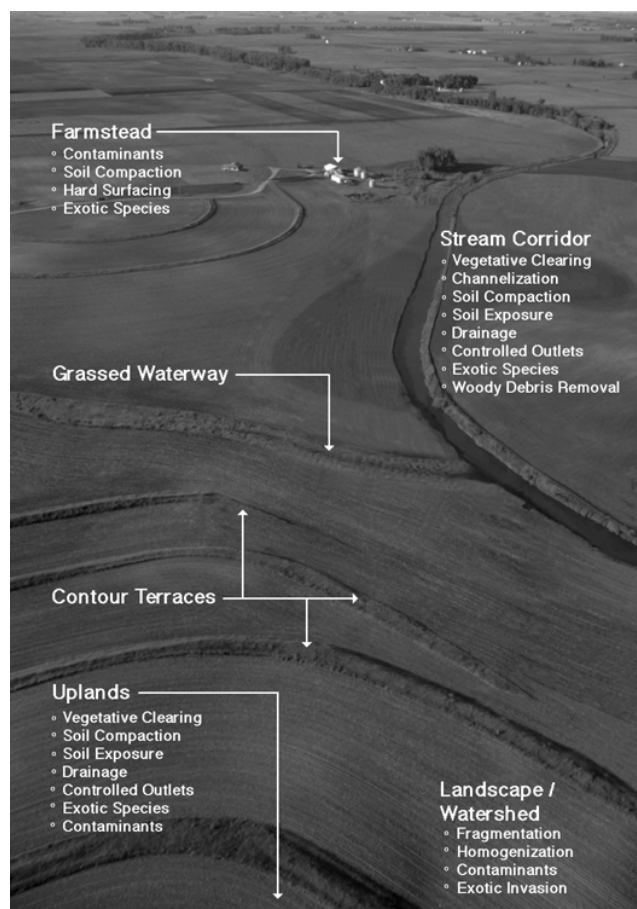
harmony with ecological processes that extend across all landscapes becomes more of an imperative than an ideal. Furthermore, conservation provisions of the 1996 Farm Bill and accompanying endeavors such as the National Conservation Buffer Initiative (NRCS 1997) offer flexibility to care for the land as never before. The following land use scenario attempts to express this flexibility in the context of comprehensive, locally led conservation work, including stream corridor restoration.

This scenario offers a brief glimpse into a hypothetical agricultural setting where the potential results of stream corridor restoration might begin to

Figure 8.53:
Hypothetical
conditions.
Activities causing
change in this
agricultural setting.

take form. Computer-generated simulations are used to graphically illustrate potential changes brought about by restoration work and associated comprehensive, on-farm conservation planning. It focuses, conceptually, on vegetative clearing, instream modifications, soil exposure and compaction, irrigation and drainage, and sediment or contaminants as the most disruptive activities associated with agricultural land use. Although an agricultural landscape typical of the Midwest was selected for illustrative purposes, the concepts shown can apply in different agricultural settings.

Hypothetical Existing Conditions

Reminiscent of the highly disruptive agricultural activities discussed in Chapter 3, **Figure 8.53** illustrates hypothetical conditions that focus primarily on production agriculture. Although functionally isolated contour terraces and a waterway have been installed in the nearby cropland, the scene depicts an ecologically deprived landscape. Many of the potential disturbance activities and subsequent changes outlined in Chapter 3 come to mind. Those hypothetically reflected in the figure are highlighted in **Table 8.10**.

Hypothetical Restoration Response

Previous sections of this chapter and earlier chapters identified connectivity and dimension (width) as important structural attributes of stream corridors. Nutrient and water flow, sediment trapping during floods, water storage, movement of flora and fauna, species diversity, interior habitat conditions, and provision of organic

Table 8.10: Summary of prominent agriculturally related disturbance activities and potential effects.

Legend: D = Activity has potential for direct impact. I = Activity has potential for indirect impact.

Potential Effects	Vegetative Clearing	Channelization	Streambed Disturbance	Soil Exposure or Compaction	Contaminants	Woody Debris Removal	Piped Discharge/Cont.Outlets
Decreased landscape diversity	D	D	I	I	I	I	I
Point source pollution	I	I	I	I	D	I	D
Nonpoint source pollution	D	D	D	I	D	D	D
Dense compacted soil	D	I	I	D	I	I	I
Increased upland surface runoff	D	I	I	D	I	I	I
Increased sheetflow with surface erosion rill and gully flow	D	I	I	D	I	I	I
Increased levels of fine sediment and contaminants in stream corridor	D	D	D	D	D	D	D
Increased soil salinity	I	I	I	I	D	I	I
Increased peak flood elevation	D	D	I	D	I	D	D
Increased flood energy	D	D	D	D	I	D	D
Decreased infiltration of surface runoff	D	D	I	D	I	D	D
Decreased interflow and subsurface flow to and within the stream corridor	D	D	I	D	D	I	D
Reduced ground water recharge and aquifer volumes	D	I	I	D	I	I	D
Increased depth to ground water	D	D	I	I	I	I	I
Decreased ground water inflow to stream	D	D	I	D	I	I	D
Increased flow velocities	D	D	D	I	I	D	D
Reduced stream meander	I	D	D	I	I	D	I
Increased or decreased stream stability	D	D	D	D	I	D	D
Increased stream migration	D	D	I	D	I	I	I
Channel widening and downcutting	D	D	D	I	I	D	D
Increased stream gradient and reduced energy dissipation	I	D	D	D	I	D	D
Increased flow frequency	D	I	I	D	D	D	D
Reduced flow duration	D	D	D	D	I	D	D
Decreased capacity of floodplain and upland	D	I	I	D	D	D	I
Increased sediment and contaminants	D	I	I	D	D	D	D
Decreased capacity of stream	I	D	D	I	D	D	D
Reduced stream capacity to assimilate nutrients/pesticides	D	D	D	D	D	D	D
Confined stream channel with little opportunity for habitat development	I	D	D	I	I	I	I
Increased streambank erosion and channel scour	D	D	D	D	I	D	D
Increased bank failure	D	D	I	D	I	D	D
Loss of instream organic matter and related decomposition	D	D	D	D	D	D	D
Increased instream sediment, salinity, or turbidity	D	D	D	I	D	D	D
Increased instream nutrient enrichment, sedimentation, and contaminants leading to eutrophication	D	I	D	D	D	D	D

■ Activity has potential for direct impact. ▨ Activity has potential for indirect impact.

Table 8.10: Summary of prominent agriculturally related disturbance activities and potential effects (continued).

Potential Effects	Existing Disturbance Activities						
	Vegetative Clearing	Channelization	Streambed Disturbance	Soil Exposure or Compaction	Contaminants	Woody Debris Removal	Piped Discharge/Cont.Outlets
Highly fragmented stream corridor with reduced linear distribution of habitat and edge effect	■	■	▫	▫	▫	■	▫
Loss of edge and interior habitat	■	■	■	▫	▫	■	▫
Decreased connectivity and dimension (width) within corridor and to associated ecosystems	■	■	■	▫	▫	▫	▫
Decreased movement of flora and fauna species for seasonal migration, dispersal repopulation	■	■	■	▫	▫	▫	▫
Reduced stream capacity to assimilate nutrients/ pesticides	■	■	■	■	■	■	■
Increase of opportunistic species, predators	■	■	▫	▫	■	■	■
Increase exposure to solar radiation, weather, and temperature	■	■	■	■	▫	■	▫
Magnified temperature and moisture extremes in corridor	■	■	■	■	▫	■	▫
Loss of riparian vegetation	■	■	■	■	■	■	■
Decrease source of in stream shade, detritus, food, and cover	■	■	■	▫	▫	▫	■
Loss of edge diversity	■	■	■	▫	▫	■	▫
Increased water temperature	■	■	■	▫	▫	■	■
Impaired aquatic habitat	■	■	■	▫	■	■	▫
Reduced invertebrate population	■	■	■	▫	■	■	■
Loss of wetland function	▫	■	■	▫	▫	▫	▫
Reduced instream oxygen	▫	■	■	▫	■	■	■
Invasion of exotic species	■	■	■	▫	▫	▫	▫
Reduced gene pool	■	■	■	▫	▫	■	■
Reduced species diversity	■	■	■	■	▫	▫	■

■ Activity has potential for direct impact.   ▫ Activity has potential for indirect impact.

materials to aquatic communities were described as just a few of the functional conditions affected by these structural attributes. Continuous indigenous vegetative cover across the widest possible stream corridor was generally identified as the most conducive to serving the broadest range of functions. This discussion went on to suggest that a long, wide stream corridor with contiguous vegetative cover is a favored overall characteristic. A contiguous, wide stream corridor may be unachievable, however, where competing land uses prevail. Furthermore, gaps caused by disturbances (utility crossings, highways and access lanes, floods, wind, fire, etc.) are commonplace.

Restoration design should establish functional connections within and external to stream corridors. Landscape elements such as remnant patches of riparian vegetation, prairie, or forest exhibiting diverse or unique vegetative communities; productive land that can support ecological functions; reserve or abandoned land; associated wetlands or meadows; neighboring springs and stream systems; ecologically innovative residential areas; and movement corridors for flora and fauna (field borders, windbreaks, waterways, grassed terraces, etc.) offer opportunities to establish these connections. An edge (transition zone) that gradually changes from one land use into another will soften environmental gradients and minimize disturbance.

With these and the broad design guidelines presented in previous sections of this chapter in mind, **Figure 8.54** presents a conceptual computer-generated illustration of hypothetical restoration results. **Table 8.11** identifies some of restoration measures hypothetically implemented and their potential effects on restoring conditions within the stream corridor and surrounding landscape.

Figure 8.54: Hypothetical restoration response.

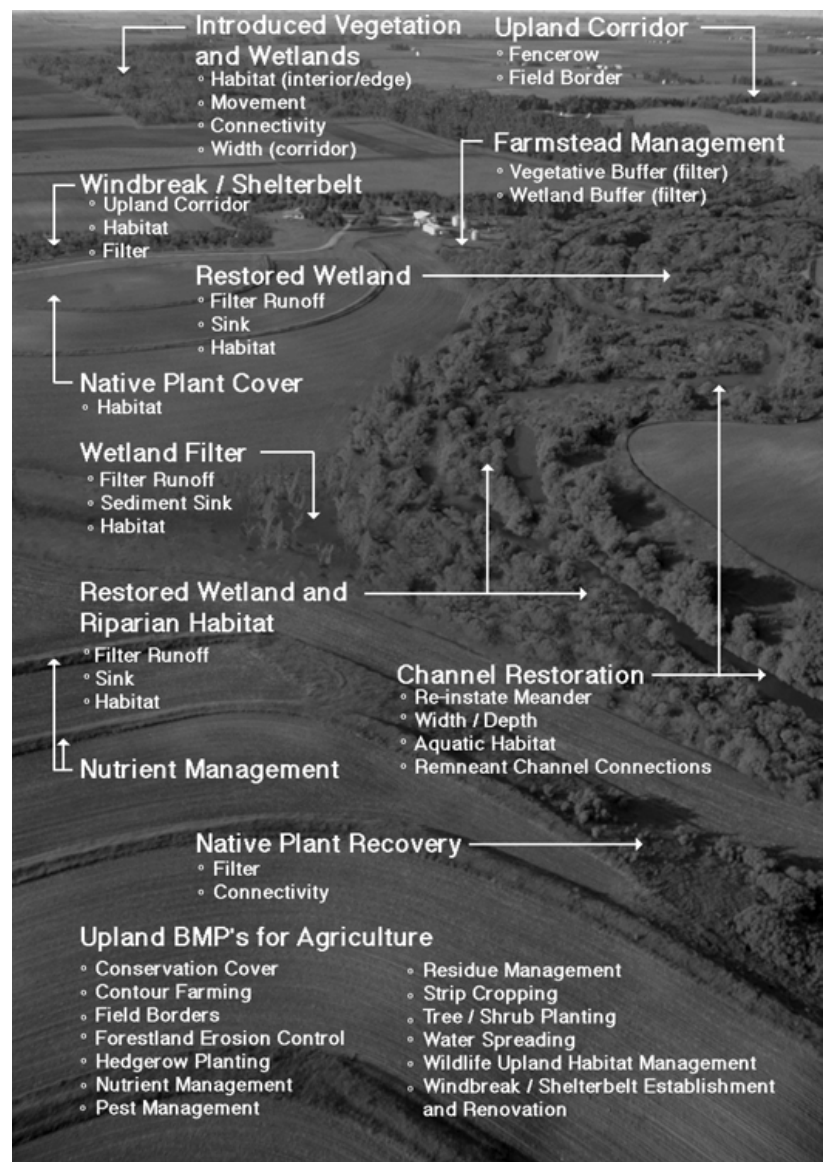*Possible results of stream corridor restoration are presented in this computer-altered photograph.*

Table 8.11: Summary of prominent restoration measures and potential resulting effects.

Potential Resulting Effects	Wetlands	Riparian Habitat	Upland Corridors	Windbreaks/Shelterbelts	Native Plant Cover	Stream Channel Restoration	Upland BMPs for Agriculture
Increased landscape diversity	■	■	■	■	■	■	■
Increased stream order	▫	▫	▫	▫	▫	■	▫
Reduced point source pollution	■	▫	▫	▫	▫	▫	▫
Reduced nonpoint source pollution	■	■	■	■	■	■	■
Increased soil friability	▫	▫	▫	▫	■	■	■
Decreased upland surface runoff	▫	▫	▫	■	■	▫	■
Decreased sheetflow, width, surface erosion, rill and gully flow	▫	▫	■	■	■	▫	■
Decreased levels of fine sediment and contaminants in stream corridor	■	■	■	■	■	▫	■
Decreased soil salinity	▫	■	▫	▫	■	▫	■
Decreased peak flood elevation	■	■	■	■	■	■	■
Decreased flood energy	■	■	■	■	■	■	■
Increased infiltration of surface runoff	■	■	■	■	■	■	■
Increased interflow and subsurface flow to and within stream corridor	■	■	▫	▫	■	■	■
Increased ground water recharge and aquifer volumes	■	■	■	■	■	■	■
Decreased depth to ground water	■	■	■	■	■	■	■
Increased ground water inflow to stream	■	■	■	■	■	■	■
Decreased flow velocities	■	■	■	■	■	■	■
Increased stream meander	▫	▫	▫	▫	▫	■	▫
Increased stream stability	■	■	■	■	■	■	■
Decreased stream migration	■	■	■	▫	■	■	■
Reduced channel widening and downcutting	■	■	■	▫	■	■	■
Decreased stream gradient and increased energy dissipation	■	■	▫	▫	▫	■	■
Decreased flow frequency	■	■	■	▫	■	▫	■
Increased flow duration	■	■	■	■	■	■	■
Increased capacity of floodplain and upland	■	■	■	■	■	▫	■
Decreased sediment and contaminants	■	■	■	■	■	▫	■
Increased capacity of stream	■	■	▫	▫	■	■	▫
Increased stream capacity to assimilate nutrients/pesticides	■	■	▫	▫	■	■	▫
Enhanced stream channel with more opportunity for habitat development	■	■	▫	▫	■	■	▫
Decreased streambank erosion and channel scour	■	■	▫	▫	■	■	▫
Decreased bank failure	■	■	▫	▫	▫	▫	▫
Gain of instream organic matter and related decomposition	■	■	▫	▫	▫	■	▫
Decreased instream sediment, salinity, or turbidity	■	■	■	■	■	■	■

■ Measure contributes directly to resulting effect.   ▫ Measure contributes little to resulting effect.

Table 8.11: Summary of prominent restoration measures and potential resulting effects (continued).

Potential Resulting Effects	Wetlands	Riparian Habitat	Upland Corridors	Windbreaks/Shelterbelts	Native Plant Cover	Stream Channel Restoration	Upland BMPs for Agriculture
Decreased instream nutrient enrichment, siltation, and contaminants leading to eutrophication	■	■	■	■	■	■	■
Connected stream corridor with increased linear distribution of habitat and edge effect	■	■	□	□	■	■	■
Gain of edge and interior habitat	■	■	■	■	■	■	■
Increased connectivity and dimension (width) within corridor and to associated ecosystems	■	■	■	■	■	■	■
Increased movement of flora and fauna species for seasonal migration, dispersal repopulation	■	■	■	■	■	■	■
Decrease of opportunistic species, predators	■	■	□	□	■	■	■
Decreased exposure to solar radiation, weather, and temperature	■	■	■	■	■	■	■
Decreased temperature and moisture extremes in corridor	■	■	■	■	■	■	■
Increased riparian vegetation	■	■	□	□	■	■	■
Increased source of in stream shade, detritus, food, and cover	■	■	□	□	■	■	■
Increase of edge diversity	■	■	■	■	■	■	■
Decreased water temperature	■	■	■	■	■	■	■
Enhanced aquatic habitat	■	■	□	□	■	■	□
Increased invertebrate population	■	■	□	□	□	■	■
Increased wetland function	■	■	□	□	□	■	■
Increased instream oxygen	■	■	■	■	■	■	■
Decrease of exotic species	■	■	□	□	■	□	■
Increased gene pool	■	■	■	■	■	■	■
Increased species diversity	■	■	■	■	■	■	■

■ Measure contributes directly to resulting effect.   □ Measure contributes little to resulting effect.

Forestry

Stream corridors are a source of large volumes of timber. Timber harvesting and related forest management practices in riparian corridors often necessitate stream corridor restoration. Forest management may be an ongoing land use and part of the restoration effort. Regardless, accessing and harvesting timber affects streams in many ways including:

- Alteration of soil conditions.
- Removal of the forest canopy.
- Reduction in the potential supply of large organic (woody) debris (Belt et al. 1992).

Forest Roads

The vast majority of the restoration design necessary following timber harvest is usually devoted to the road system, where the greatest alteration of soil conditions has taken place. Inadequate drainage, poor location, improperly sized and maintained

BMP Implementation and Section 319 of the Clean Water Act

Section 319 of the Clean Water Act of 1987 required the states to identify and submit BMPs for USEPA approval to help control nonpoint sources of pollution. As of 1993, 41 of 50 states had EPA-approved voluntary or regulatory BMP programs dealing with silvicultural (forest management) activities. The state BMPs are all similar; the majority deal with roads. Montana, for example, has a total of 55 specifically addressed forest practices. Of those 55 practices, 35 deal with road planning and location, road design, road maintenance, road drainage, road construction, and stream crossings.

culverts, and lack of erosion control measures on road prisms, cut-and-fill slopes, and ditches are problems common to a poor road design (Stoner and McFall 1991). The most extreme road system rehabilitation requires full road closure. Full road closure involves removal of culverts and restoration of the streams that were crossed. It can also involve the ripping or tilling of road surfaces to allow plant establishment. If natural vegetation has not already invaded areas of exposed soils, planting and seeding might be necessary.

Full closure might not be a viable alternative if roads are needed to provide access for other uses. In these circumstances a design to restrict traffic might be appropriate. Voluntary traffic control usually cannot be relied on, so traffic barriers like gates, fences, or earth berms could be necessary. Even with traffic restriction, roads require regular inspection for existing or potential maintenance needs. The best time for inspection is during or immediately after large storms or snowmelt episodes so the effectiveness of the culverts and road drainage features can be witnessed first-hand. Design should address regular maintenance activities including road grading, ditch cleaning, culvert cleaning, erosion control vegetation establishment, and vegetation management.

Buffer Strips in Forestry

Forested buffer strips are generally more effective in reducing sediment and chemical loadings in the stream corridor than vegetated filter strips (VFS). However, they are susceptible to similar problems with concentrated

flows. Buffers constructed as part of a conservation system increase effectiveness. A stiff-stemmed grass hedge could be planted upslope of either a VFS or a woody riparian forest buffer. The stiff-stemmed grass hedge keeps sediment out of the buffer and increases shallow sheet flow through the buffer.

Most state BMPs also have special sections devoted to limitations for forest management activities in riparian "buffer strips" (also referred to as Streamside Management Zones or Streamside Protection Zones).

Budd et al. (1987) developed a procedure for determining buffer widths for streams within a single watershed in the Pacific Northwest. They focused their attention primarily on mainte-

nance of fish and wildlife habitat quality (stream temperature, food supply, stream structure, sediment control) and found that effective buffer widths varied with the slope of adjacent uplands, the distribution of wetlands, soil and vegetation characteristics, and land use. They concluded that practical determinations of stream buffer width can be made using such analyses, but it is clear that a generic buffer width which would provide habitat maintenance while satisfying human demands does not exist. The determination of buffer widths involves a broad perspective that integrates ecological functions and land use. The section on design approaches to common effects at the beginning of this chapter also includes some discussion on stream buffer width.

Table 8.12: Buffer strip requirements by state.

State	Stream Class	Buffer Strip Requirements		
		Width	**Shade or Canopy**	**Leave Trees**
Idaho	**Class I***	Fixed minimum (75 feet)	75% current shade[a]	Yes, number per 1000 feet, dependent on stream width[b]
	Class II*	Fixed minimum (5 feet)	None	None
Washington	**Type 1, 2, and 3***	Variable by stream width (5 to 100 feet)	50%, 75% if temperature > 60°F	Yes, number per 1000 feet, dependent on stream width and bed material
	Type 4*	None	None	25 per 1000 feet, 6 inches diameter
California	**Class I and Class II***	Variable by slope and stream class (50 to 200 feet)	50% overstory and/or understory; dependent on slope and stream class	Yes; number to be determined by canopy density
	Class III*	None[b]	50% understory[e]	None[e]
Oregon	**Class I***	Variable, 3 times stream width (25 to 100 feet)	50% existing canopy, 75% existing shade	Yes; number per 1000 feet and basal area per 1000 feet by stream width
	Class II special protection*	None[f]	75% existing shade	None

* Human water supply or fisheries use.

** Streams capable of sediment transport (CA) or other influences (ID and WA) or significant impact (OR) on downstream waters.

[a] In ID, the shade requirement is designed to maintain stream temperatures.

[b] In ID, the leave tree requirement is designed to provide for recruitment of large woody debris.

[c] May range as high as 300 feet for some types of timber harvest.

[d] To be determined by field inspection.

[e] Residual vegetation must be sufficient to prevent degradation of downstream beneficial uses.

[f] In eastern OR, operators are required to "leave stabilization strips of undergrowth... sufficient to prevent washing of sediment into Class I streams below."

Pacific Northwest Floods Of 1996

Floods, Landslides, and Forest Management—'The Rest of The Story'

Warm winds, intense rainfall, and rapid snowmelt during the winter of 1995-96 and again in the winter of 1996-97 caused major flooding, landslides, and related damage throughout the Pacific Northwest (**Figure 8.55**). Such flooding had not been seen for more than 30 years in hard-hit areas. Damage to roads, campgrounds, trails, watersheds, and aquatic resources was widespread on National Forest Service lands. These events offered a unique opportunity to investigate the effects of severe weather, examine the influence and effectiveness of various forest management techniques, and implement a repair strategy consistent with ecosystem management principles.

The road network in the National Forests was heavily damaged during the floods. Decisions about the need to replace roads are based on long-term access and travel requirements. Relocation of roads to areas outside floodplains is a measure being taken. Examination of road crossings at streams concluded with design recommendations to keep the water moving, align culverts horizontally and longitudinally with the stream channel, and minimize changes in stream channel cross section at inlet basins to prevent debris plugs.

Many river systems were also damaged. In some systems, however, stable, well-vegetated slopes and streambanks combined with fully functioning floodplains buffered the effects of the floods. Restoration efforts will focus on aiding natural processes in these systems. Streambank stabilization and riparian plantings will be commonly used. Examination of instream structure durability concluded that structures are more likely to remain in place if they are in fourth-order or smaller streams and are situated in a manner that maintains a connection between the structure and the streambank. They will be most durable in watersheds with low landslide/debris torrent frequency.

Figure 8.55: 1996 Landslides.
(a) April landslide: debris took out the track into the Greenwater River and (b) July landslide: debris took out the road and deposited debris into the river.

(a)

(b)

Stream corridors have varied dimensions, but stream buffer strips have legal dimensions that vary by state (**Table 8.12**). The buffer may be only part of the corridor or it may be all of it. Unlike designing stream corridors for recreation features or grazing use, designing for timber harvest and related forest management activities is quite regimented by law and regulation. Specific requirements vary from state to state; the state Forester's office or local Extension Service can provide guidance on regulatory issues. USDA Natural Resource Conservation Service offices and Soil and Water Conservation District offices also are sources of information. Refer to Belt et al. (1992) and Welsch (1991) for guidance on riparian buffer strip design, function, and management. Salo and Cundy (1987) provide information on forestry effects on fisheries.

Grazing

The closer an ecosystem is managed to allow for natural ecological processes to function, the more successful a restoration strategy will be. In stream corridors that have been severely degraded by grazing, rehabilitation should begin with grazing management to allow for vegetative recovery.

Vegetative recovery is often more effective than installing a structure. The vegetation maintains itself in perpetuity, allows streams to function in ways that artificial structures cannot replicate, and provides resiliency that allows riparian systems to withstand a variety of environmental conditions (Elmore and Beschta 1987).

Designs that promote vegetative recovery after grazing are beneficial in a number of ways. Woody species can provide resistance to channel erosion and improve channel stability so that other species can become established. As vegetation becomes established, channel elevation will increase as sediment is deposited within and along the banks of the channel (aggradation), and water tables will rise and may reach the root zone of plants on former terraces or floodplains. This aggradation of the channel and the rising water table allow more water to be stored during wet seasons, thereby prolonging flow even during periods of drought (Elmore and Beschta 1987).

Kauffman et al. (1993) observed that fencing livestock out of the riparian zone is the only grazing strategy that consistently results in the greatest rate of vegetative recovery and the greatest improvement in riparian function. However, fencing is very expensive, requires considerable maintenance,

and can limit wildlife access—a negative impact on habitat or conduit functions.

Some specialized grazing strategies hold promise for rehabilitating less severely impacted riparian and wetland areas without excluding livestock for long periods of time. The efficiency of a number of grazing strategies with respect to fishery needs are summarized in **Tables 8.13** and **8.14** (from Platts 1989). They summarize the influence of grazing systems and stream system characteristics on vegetation response, primarily from a western semiarid perspective. Some general design recommendations for selecting a strategy include the following (Elmore and Kauffmann 1994):

- Each strategy must be tailored to a particular stream or stream reach. Management objectives and components of the ecosystem that are of critical value must be identified (i.e., woody species recovery, streambank restoration, increased habitat diversity, etc.). Other information that should be identified includes present vegetation, potential of the site for recovery, the desired future condition, and the current factors causing habitat degradation or limiting its recovery.

- The relationships between ecological processes that must function for riparian recovery should be described. Factors affecting present condition (i.e., management stress vs. natural stress) and conditions required for the stream to resume natural functions need

Table 8.13:
Evaluation and rating
of grazing strategies.

Strategy[a]	Level to Which Riparian Vegetation is Commonly Used	Control of Animal Distribution (Allotment)	Streambank Stability	Brushy Species Condition	Seasonal Plant Regrowth	Stream Riparian Rehabilitation Potential	Fishery Needs Rating[b]
Continuous season-long (cattle)	Heavy	Poor	Poor	Poor	Poor	Poor	1
Holding (sheep or cattle)	Heavy	Excellent	Poor	Poor	Fair	Poor	1
Short duration-high intensity (cattle)	Heavy	Excellent	Poor	Poor	Poor	Poor	1
Three herd-four pasture (cattle)	Heavy to moderate	Good	Poor	Poor	Poor	Poor	2
Holistic (cattle or sheep)	Heavy to light	Good	Poor to good	Poor	Good	Poor to excellent	2-9
Deferred (cattle)	Moderate to heavy	Fair	Poor	Poor	Fair	Fair	3
Seasonal suitability (cattle)	Heavy	Good	Poor	Poor	Fair	Fair	3
Deferred-rotation (cattle)	Heavy to moderate	Good	Fair	Fair	Fair	Fair	4
Stuttered deferred-rotation (cattle)	Heavy to moderate	Good	Fair	Fair	Fair	Fair	4
Winter (sheep or cattle)	Moderate to heavy	Fair	Good	Fair	Fair to good	Good	5
Rest-rotation (cattle)	Heavy to moderate	Good	Fair to good	Fair	Fair to good	Fair	5
Double rest-rotation (cattle)	Moderate	Good	Good	Fair	good	Good	6
Seasonal riparian preference (cattle or sheep)	Moderate to light	Good	Good	Good	Fair	Fair	6
Riparian pasture (cattle or sheep)	As prescribed	Good	Good	Good	Good	Good	8
Corridor fencing (cattle or sheep)	None	Excellent	Good to excellent	Good to excellent	Good	Excellent	9
Rest-rotation with seasonal preference (sheep)	Light	Good	Good to excellent	Good to excellent	Good	Excellent	9
Rest or closure (cattle or sheep)	None	Excellent	Excellent	Excellent	Excellent	Excellent	10

[a] Jacoby (1989) and Platts (1989) define these management strategies
[b] Rating scale based on 1 (poorly compatible) to 10 (highly compatible with fishery needs)

Table 8.14: Generalized relationships between grazing systems, stream system characteristics, and riparian vegetation response.

Grazing System	Steep Low Sediment Load	Steep High Sediment Load	Moderate Low Sediment Load	Moderate High Sediment Load	Flat Low Sediment Load	Flat High Sediment Load
No grazing	Shrubs + Herbs + Banks 0	Shrubs + Herbs + Banks 0 to +	Shrubs + Herbs + Banks 0	Shrubs + Herbs + Banks +	Shrubs + Herbs + Banks +	Shrubs + Herbs + Banks +
Winter or dormant season	Shrubs + Herbs + Banks 0	Shrubs + Herbs + Banks 0 to +	Shrubs + Herbs + Banks +	Shrubs + Herbs + Banks +	Shrubs + Herbs + Banks +	Shrubs + Herbs + Banks +
Early growing season	Shrubs + Herbs + Banks 0	Shrubs + Herbs + Banks 0 to +	Shrubs + Herbs + Banks +	Shrubs + Herbs + Banks +	Shrubs + Herbs + Banks +	Shrubs + Herbs + Banks +
Deferred or late season	Shrubs – Herbs + Banks 0 to -	Shrubs – Herbs + Banks 0 to -	Shrubs – Herbs + Banks 0 to +	Shrubs – Herbs + Banks +	Shrubs – Herbs + Banks +	Shrubs – Herbs + Banks +
Three-pasture rest rotation	Shrubs – Herbs + Banks 0 to –	Shrubs – Herbs + Banks 0 to –	Shrubs – Herbs + Banks 0 to +	Shrubs – Herbs + Banks +	Shrubs – Herbs + Banks +	Shrubs – Herbs + Banks +
Deferred rotation	Shrubs – Herbs + Banks 0 to –	Shrubs – Herbs + Banks 0 to –	Shrubs – Herbs + Banks + to 0	Shrubs – Herbs + Banks +	Shrubs – Herbs + Banks +	Shrubs + Herbs + Banks +
Early rotation	Shrubs + Herbs + Banks 0 to –	Shrubs + Herbs + Banks 0 to +	Shrubs + Herbs + Banks + to 0	Shrubs + Herbs + Banks +	Shrubs + Herbs + Banks +	Shrubs + Herbs + Banks +
Rotation	Shrubs – Herbs + Banks 0 to –	Shrubs – Herbs + Banks 0 to –	Shrubs – Herbs + Banks 0 to +	Shrubs – Herbs + Banks +	Shrubs – Herbs + Banks +	Shrubs – Herbs + Banks +
Season-long	Shrubs – Herbs – Banks 0 to –	Shrubs – Herbs – Banks 0 to –	Shrubs – Herbs – Banks –	Shrubs – Herbs – Banks –	Shrubs – Herbs – Banks –	Shrubs – Herbs – Banks –
Spring and fall	Shrubs – Herbs – Banks 0 to –	Shrubs – Herbs – Banks 0 to –	Shrubs – Herbs – Banks –	Shrubs – Herbs – Banks –	Shrubs – Herbs – Banks – to 0	Shrubs – Herbs – Banks 0 to +
Spring and summer	Shrubs – Herbs – Banks 0 to –	Shrubs – Herbs – Banks 0 to –	Shrubs – Herbs – Banks –	Shrubs – Herbs – Banks – to 0	Shrubs – Herbs – Banks – to 0	Shrubs – Herbs – Banks 0 to +

Note: – = decrease; + = increase; 0 = no change. Stream gradient: 0 to 2% = flat; 2 to 4% = moderate; > 4% = steep. Banks refers to bank stability.

to be assessed. Anthropogenic factors causing stream degradation must be identified and changed.

- Design and implementation should be driven by attainable goals, objectives, and management activities that will achieve the desired structure and functions.

- Implementation should include a monitoring plan that will evaluate management, allowing for corrections or modifications as necessary, and a strong compliance and use supervision program.

The main consideration for selecting a grazing system is to have an adequate vegetative growing season between the period of grazing and timing of high-energy runoff. It is impossible to provide a cookie-cutter grazing strategy for every stream corridor; designs have to be determined on the ground, stream by stream, manager by manager. Simply decreasing the number of livestock is not a solution to degraded riparian conditions; rather, restoring these degraded areas requires fundamental changes in the ways that livestock are grazed (Chaney et al. 1990).

Clearly, the continued use of grazing systems that do not include the functional requirements of riparian vegetation communities will only perpetuate riparian problems (Elmore and Beschta 1987). Kinch (1989) and Clary and Webster (1989) provide greater detail on riparian grazing management and designing alternative grazing strategies. Chaney and others (1990 and 1993) present photo histo-

ries of a number of interesting grazing restoration case studies, and of the short-term results of some of the available grazing strategies.

Mining

Post-mining reclamation of stream corridors must begin with restoration of a properly functioning channel. Because many of the geologic and geomorphic controls associated with the pre-disturbance channel may have been obliterated by mining operations, design of the post-mining channel often requires approaches other than mimicking the pre-disturbance condition. Channel alignment, slope, and size may be determined on the basis of empirical relations developed from other streams in the same hydrologic and physiographic settings (e.g., Rechard and Schaefer 1984, Rosgen 1996). Others (e.g., Hasfurther 1985) have used a combination of empirical and theoretical approaches for design of reclaimed channels. Total reconstruction of stream channels is treated at length in Section 8.E. Other sections of the chapter address stabilization of streambanks, revegetation of floodplains and terraces, and restoration of aquatic and terrestrial habitats. Additional guidance is available in Interfluve, Inc. (1991).

Surface mining is usually associated with large-scale disturbances in the contributing watershed, therefore, a rigorous hydrological analysis of pre- and post-mining conditions is critical for stream corridor restoration of disturbed systems. The hydrologic analysis should include a frequency analysis of extreme high- and low-flow events to assess channel performance in the post-mining landscape.

Oven Run, Pennsylvania

The effects of abandoned mines draining into the surrounding lands cause dramatic changes in the area (**Figure 8.58(a)**). Runoff with high levels of minerals and acidity can denude the ground of vegetation, expose the soil, and allow erosion with the sediment further stressing streams and wetland. Any efforts to restore streams in this environment must deal with the problem if any success is to be likely.

The Natural Resources Conservation Service, formerly known as the Soil Conservation Service, has been working on the Oven Run project along with the Stonycreek Conemaugh River Improvement (SCRIP) to improve water quality in a 4-mile reach above the Borough of Hooversville. SCRIP is a group of local and state government as well as hundreds of individuals interested in improving the water quality in an area on Pennsylvania's Degraded Watersheds list.

The initial goal of improving water quality resulted in improving habitat and aesthetic qualities. The water coming into Hooversville had higher-than-desired levels of iron, manganese, aluminum, sulfate, and acidity. Six former strip mines, which had a range of problems, were identified. They included deep mine openings that have large flows of acid mine drainage, acid mine seepage into streams, eroding spoil areas, areas of ponded water that infiltrate into ground water (adding to the acid mine drainage), and areas downhill of seepage and deep mine drainage that are denuded and eroding.

Control efforts included grading and vegetating the abandoned mine to reduce infiltration through acid-bearing layers and reduce erosion and sedimentation, surface water controls to carry water around the sites to safer outlets, and treating discharge flow with anoxic limestone drains and chambered passive wetland treatments (**Figure 8.58(b))**. Additionally, 1,000 feet of trees were planted along one of the site streams to shade the Stoneycreek River. Average annual costs for the six sites were estimated to be $503,000 compared to average annual benefits of $513,000.

The sites are being monitored on a monthly basis, and 4 years after work was begun the treatments have had a measurable success. The acid influent has been neutralized, and the effluent is now a net alkaline. Iron, aluminum, and manganese levels have been reduced, with iron now at average levels of 0.5 mg/L from average levels of 35 mg/L.

(a)

(b)

Figure 8.58: Stream corridor *(a)* before and *(b)* after restoration.

Hydrologic modeling may be required to generate runoff hydrographs for the post-mining channel because watershed geology, soils, vegetation, and topography may be completely altered by mining operations. Thus, channel design and stability assessments will be based on modeled runoff rates reflecting expected watershed conditions. The hydrologic analysis for post-mining restoration should also address sediment production from the reclaimed landscape. Sediment budgets (see Chapter 7) will be needed for both the period of vegetation establishment and the final revegetated condition.

The hydrologic analyses will provide restoration practitioners with the flow and sediment characteristics needed for restoration design. The analyses may also indicate a need for at least temporary runoff detention and sediment retention during the period of vegetation establishment. However, the post-mining channel should be designed for long-term equilibrium with the fully reclaimed landscape.

Water quality issues (e.g., acid mine drainage) often control the feasibility of stream restoration in mined areas and should be considered in design.

Figure 8.56: Controlled access
Control of streambank access is an important part of the restoration design.
Source: J. McShane.

Recreation

Both concentrated and dispersed recreational use of stream corridors can cause damage and ecological change. Ecological damage primarily results from the need for access for the recreational user. A trail often will develop along the shortest or easiest route to the point of access on the stream. Additional resource damage may be a function of the mode of access to the stream: motorcycles and horses cause far more damage to vegetation and trails than do pedestrians. Control of streambank access in developed recreation sites must be part of a restoration design. On undeveloped or unmanaged sites, such control is more difficult but still very necessary (**Figure 8.56**).

Rehabilitation of severely degraded recreation areas may require at least temporary use restrictions. Even actively eroding trails, camp and picnic sites, and stream access points can be stabilized through temporary site closure and combinations of soil and vegetation restoration (Wenger 1984, Marion and Merriam 1985, Hammitt and Cole 1987). Closure will not provide a long-term solution if access is restored without addressing the cause of the original problem. Rather, new trails and recreation sites should be located and constructed based on an understanding of vegetation capabilities, soil limitations, and other physical site characteristics. Basically, the keys to a successful design are:

- Initially locating or moving use to the most damage-resistant sites.

- Influencing visitor use.
- Hardening use areas to make them more resistant.
- Rehabilitating closed sites.

Urbanization

Few land uses have the capacity to alter water and sediment yield from a drainage as much as the conversion of a watershed from rural to urban conditions; thus, few land uses have greater potential to affect the natural environment of a stream corridor.

As a first step in hydrologic analyses, designers should characterize the nature of existing hydrologic response and the likelihood for future shifts in water and sediment yield. Initially, construction activities create excess sediment that can be deposited in downstream channels and floodplains. As impervious cover increases, peak flows increase. Water becomes cleaner as more area is covered with landscaping or impervious material. The increased flows and cleaner water enlarge channels, which increases sediment loads downstream.

Determine if the watershed is (a) fully urbanized, (b) undergoing a new phase of urbanization, or (c) is in the beginning stages of urbanization (Riley, 1998).

An increase in the amount of impervious cover in a watershed leads to increased peak flows and resulting channel enlargement (**Figure 8.57**). Research has shown that impervious cover of as little as 10 to 15 percent of a watershed can have significant adverse effects on channel conditions (Schueler 1996). Magnitudes of channel-forming or bankfull flood

events (typically 1- to 3-year recurrence intervals) are increased significantly, and flood events that previously occurred once every year or two may occur as often as one or two times a month.

Enlargement of streams with subsequent increases in downstream sediment loads in urbanized watersheds should be expected and accommodated in the design of restoration treatments. Procedures for estimating peak discharges are described in Chapter 7, and effects of urbanization on magnitude of peak flows must be incorporated into the analysis. Sauer et al. (1983) investigated the effect of urbanization on peak flows by analyzing 199 urban watersheds in 56 cities and 31 states. The objective of the analysis was to determine the increase in peak discharges due to urbanization and to develop regression equations for estimating design floods, such as the 100-year or 1 percent chance annual flood, for ungauged urban watersheds. Sauer et al. (1983) developed regression equations based on watershed, climatic, and urban characteristics that can be used to

Figure 8.57: Storm water flow on a paved surface.
Impervious surfaces increase peak flows and can result in channel enlargement.
Source: M. Corrigan.

estimate the 2, 5, 10, 25, 50, 100, and 500-year urban annual peak discharges for ungauged urban watersheds. The equation for the 100-year flood in cubic feet per second (UQ100) is provided as an example:

$$UQ100 = 2.50\ A^{.29}\ SL^{.15}\ (RI2+3)^{1.76}$$
$$(ST+8)^{-.52}\ (13-BDF)^{-.28}\ IA^{.06}\ Q100^{.63}$$

where the explanatory variables are drainage area in square miles (A), channel slope in feet per mile (SL), the 2-year, 2-hour rainfall in inches (RI2), basin storage in percent (ST), basin development factor (BDF), which is a measure of the extent of development of the drainage system (dimensionless, ranging from 0 to 12), percent impervious area (IA), and the equivalent rural peak discharge in cubic feet per second (RQ100) in the example equation above.

Sauer et al. (1983) provide the allowable range for each variable. The two indices of urbanization in the equation are BDF and IA. They can be used to adjust the rural peak discharge RQ100 (either estimated or observed) to urban conditions.

Sauer et al. (1983) provide equations like the one above and graphs that relate the ratio of the urban to rural peak discharge (UQx/RQx) for recurrence intervals x = 2, 10, and 100 years. The 2-year peak ratio varies from 1.3 to 4.3, depending on the values of BDF and IA; the 10-year ratio varies from 1.2 to 3.1; and the 100-year ratio varies from 1.1 to 2.6. These ratios indicate that urbanization generally has a lesser effect on higher-recurrence-interval floods because watershed soils are more saturated and floodplain storage more fully depleted in large floods, even in the rural condition.

More sophisticated hydrologic analyses than the above are often used, including use of computer models, regional regression equations, and statistical analyses of gauge data. Hydrologic models, such as HEC-1 or TR-20, are often already developed for some urban watersheds.

Once the flood characteristics of the stream are adjusted for urbanization, new equilibrium channel dimensions can be estimated from hydraulic geometry relationships developed using data from stable, alluvial channels in similar (soils, slope, degree of urbanization) watersheds, or other analytical approaches. Additional guidance for design of restored channels is provided earlier in this chapter in the section on channel reconstruction.

Changes in flooding caused by urbanization of a watershed can be mitigated during urban planning through practices designed to control storm runoff. These practices emphasize the use of vegetation and biotechnical methods, as well as structural methods, to maintain or restore water quality and dampen peak runoff rates. Strategies for controlling runoff include the following:

- Increasing infiltration of rainfall and streamflow to reduce runoff and to remove pollutants.

- Increasing surface and subsurface storage to reduce peak flows and induce sediment deposition.

- Filtration and biological treatment of suspended and soluble pollutants (i.e., constructed wetlands).

- Establishment and/or enhancement of forested riparian buffers.

- Management of drainage from the transportation network.

- Introduction of trees, shrubs, etc., for various restoration purposes.

In addition to changes in water yield, urbanization of a watershed frequently generates changes in its sediment yield. In humid climates, vegetative cover prior to urbanization often is adequate to protect soil resources and minimize natural erosion, and the combination of impervious area and vegetation of a fully urban watershed might be adequate to minimize sediment yield. During the period of urbanization, however, sediment yields increase significantly as vegetation is cleared and bare soil is exposed during the construction process. In more arid climates, sediment yield from an urban watershed may actually be lower than the yield from a rural watershed due to the increased impervious area and vegetation associated with landscaping, but the period of urbanization (i.e., construction) is still the time of greatest sediment production.

The effect of urbanization on sediment discharge is illustrated in **Figure 8.59**, which contains data from nine subbasins in a 32-square-mile area in the Rock Creek and Anacostia River Basins north of Washington, DC (Yorke and Herb 1978). During the period of data collection (1963-74), three subbasins remained virtually

Figure 8.59: Sediment-transport curves for growing season storms. *The effect of urbanization on sediment discharge is illustrated from data collected in a 32-square-mile area.*

rural while the others underwent urban development. In 1974, urban land represented from 0 to 60 percent of land use in the nine subbasins. These data were used to develop a relation between suspended sediment yield and the percentage of land under construction. This relation indicated that suspended sediment yield increased about 3.5 times for watersheds with 10 percent of the land area under construction. However, suspended-sediment yields for watersheds where sediment controls (primarily sediment basins) were employed for 50 percent of the construction area were only about one-third of these for areas without controls. The effect of controls is seen in the figure. The three curves present growing season data for three periods of increasing sediment control: 1963-67, when no controls were used on construction sites; 1968-71, when controls were mandatory;
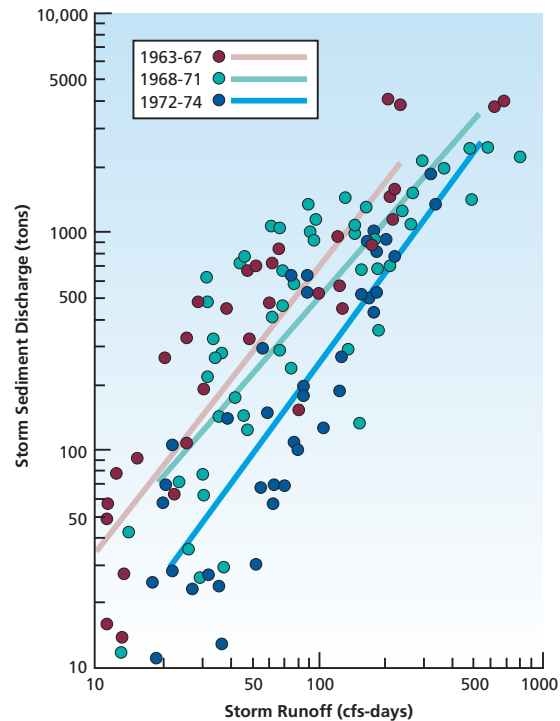
and 1972-74, when controls were mandatory and subject to inspection by county officials. It further illustrates that storm runoff is not the only factor affecting storm sediment discharge as evidenced by the significant scatter about each relation.

In addition to sediment basins, management practices for erosion and sediment control focus on the following objectives:

- Stabilizing critical areas along and on highways, roads, and streets.
- Siting and placement of sediment migration barriers.
- Design and location of measures to divert or exclude flow from sensitive areas.
- Protection of waterways and outlets.
- Stream and corridor protection and enhancement.

All of these objectives emphasize the use of vegetation for sediment control. Additional information on BMPs for controlling runoff and sediment in urban watersheds can be found in the *Techniques Appendix*.

In theory, a local watershed management plan might be the best tool to protect a stream corridor from the cumulative impact of urban development; however, in practice, few such plans have realized this goal (Schueler 1996). To succeed, such plans must address the amount of bare ground exposed during construction and the amount of impervious area that will exist during and after development of the watershed. More importantly, success will depend on using the watershed plan to guide development

decisions, and not merely archiving it as a one-time study whose recommendations were read once but never implemented (Schueler 1996).

Key Tools of Urban Stream Restoration Design

Restoration design for streams degraded by prior urbanization must consider pre-existing controls and their effects on restoration objectives. Seven restoration tools can be applied to help restore urban streams. These tools are intended to compensate for stream functions and processes that have been diminished or degraded by prior watershed urbanization. The best results are usually obtained when the following tools are applied together.

Tool 1. Partially restore the predevelopment hydrological regime. The primary objective is to reduce the frequency of bankfull flows in the contributing watershed. This is often done by constructing upstream storm water retrofit ponds that capture and detain increased storm water runoff for up to 24 hours before release (i.e., extended detention). A common design storm for extended detention is the one-year, 24 hour storm event. Storm water retrofit ponds are often critical in the restoration of small and midsized streams, but may be impractical in larger streams and rivers.

Tool 2. Reduce urban pollutant pulses. A second need in urban stream restoration is to reduce concentrations of nutrients, bacteria and toxics in the stream, as well as trapping excess sediment loads. Generally, three tools can be applied to reduce pollutant inputs to an urban stream: storm water retrofit ponds or wetlands, watershed

pollution prevention programs, and the elimination of illicit or illegal sanitary connections to the storm sewer network

Tool 3. Stabilize channel morphology. Over time, urban stream channels enlarge their dimensions, and are subject to severe bank and bed erosion. Therefore, it is important to stabilize the channel, and if possible, restore equilibrium channel geometry. In addition, it is also useful to provide undercuts or overhead cover to improve fish habitat. Depending on the stream order, watershed impervious cover and the height and angle of eroded banks, a series of different tools can be applied to stabilize the channel, and prevent further erosion. Bank stabilization measures include imbricated rip-rap, brush bundles, soil bioengineering methods such as willow stakes and bio-logs, lunker structures and rootwads. Grade stabilization measures are discussed earlier in this chapter and in Appendix A.

Tool 4. Restore Instream habitat structure. Most urban streams have poor instream habitat structure, often typified by indistinct and shallow low flow channels within a much larger and unstable storm channel. The goal is to restore instream habitat structure that has been blown out by erosive floods. Key restoration elements include the creation of pools and riffles, confinement and deepening of the low flow channels, and the provision of greater structural complexity across the streambed. Typical tools include the installation of log checkdams, stone wing deflectors and boulder clusters along the stream channel.

Tool 5. Reestablish Riparian Cover. Riparian cover is an essential component of the urban stream ecosystem. Riparian cover stabilizes banks, provides large woody debris and detritus, and shades the stream. Therefore, the fifth tool involves reestablishing the riparian cover plant community along the stream network. This can entail active reforestation of native species, removal of exotic species, or changes in mowing operations to allow gradual succession. It is often essential that the riparian corridor be protected by a wide urban stream buffer.

Tool 6. Protect critical stream substrates. A stable, well sorted streambed is often a critical requirement for fish spawning and secondary production by aquatic insects. The bed of urban streams, however, is often highly unstable and clogged by fine sediment deposits. It is often necessary to apply tools to restore the quality of stream substrates at points along the stream channel. Often, the energy of urban storm water can be used to create cleaner substrates—through the use of tools such as double wing deflectors and flow concentrators. If thick deposits of sediment have accumulated on the bed, mechanical sediment removal may be needed.

Tool 7. Allow for recolonization of the stream community. It may be difficult to reestablish the fish community in an urban stream if downstream fish barriers prevent natural recolonization. Thus, the last urban stream restoration tool involves the judgment of a fishery biologist to determine if downstream fish barriers exist, whether they can be removed, or whether selective stocking of native fish are needed to recolonize the stream reach.